Juneau, Alaska, Wind Hazard Information System (WHIS): A Wintertime Assessment of Wind Sensors on Mt. Washington, New Hampshire

William Benner Thomas Carty

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16. Abstract

The Federal Aviation Administration (FAA) Weather Branch performed a 6-week wintertime assessment of wind sensors on Mt. Washington, NH, in 1999. The purpose of the effort was to perform a preliminary investigation of the severe weather performance capabilities of anemometers for use in the prototype Wind Hazard Information System (WHIS) at Juneau International Airport, AK. The test site was selected as it is subjected to extreme meteorological and climatic conditions equivalent to alpine and arctic zones characteristic to Juneau. The summit weather is severe and often experiences snow and icing conditions, and the buildup of rime ice on exposed surfaces is prevalent and often substantial. One ultrasonic and two mechanical wind sensors, all with internal heater capabilities, were studied. Other instruments included an ice detector, a relative humidity probe, and an Internet-capable video camera which was set up to continuously monitor temperature/weather and sensor conditions. Additional equipment consisted of a datalogger, a personal computer (PC), and various communications equipment located in a heated instrument shelter. About 37 days of data were remotely collected, downloaded, and analyzed. Figures are presented in this report to document and present the test bed setup, data collection, and analysis results.

This effort was considered primarily a demonstration and shakedown effort, as a number of limitations were necessary and understood before the test bed installation. The most severe limitation was problems encountered with the video camera. Despite the test bed difficulties, a sufficient amount of useful data was successfully analyzed to draw some conclusions on the adequacy of the test bed setup and the performance of the wind sensors. Results show several effects of snow and icing on wind sensor performance. One wind direction mechanical sensor failed early in the study due to heater-related problems. The ultrasonic sensor experienced a significant amount of data outages, and was unavailable 9 percent of the time. The failures are highly correlated to snow conditions. Other data suggests the buildup of ice on the mast of the mechanical sensors is significant and affects sensor performance. Several test setup and data collection recommendations are provided in support of a proposed larger scale effort.

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EXECUTIVE SUMMARY

The Weather Branch (ACT-320) of the Federal Aviation Administration (FAA) William J. Hughes Technical Center performed a 6-week wintertime assessment of several wind sensors on Mt. Washington, NH, in February and March of 1999. The purpose of the effort was to perform a preliminary investigation of the severe weather performance capabilities of the anemometers currently used in the prototype Wind Hazard Information System (WHIS) at Juneau International Airport, AK. A sonic wind sensor considered as a possible candidate for use in the WHIS was also tested. The test bed is located near the Mt. Washington Observatory (MWO) at the summit. The site was selected as it is subjected to extreme meteorological and climatic conditions equivalent to alpine and arctic zones characteristic to Juneau. The summit weather is severe and often experiences snow and icing conditions, and the buildup of rime ice on exposed surfaces is prevalent and often substantial.

The test bed consisted of one ultrasonic and two mechanical wind sensors. All sensors had internal heater capabilities. Other weather instrumentation included an ice detection sensor and a temperature/relative humidity probe. An Internet-capable video camera was set up to continuously monitor weather and sensor conditions. Additional instrumentation and equipment consisted of a datalogger, a personal computer (PC), and various communications equipment located in a heated instrument shelter. The test bed was completely unattended during the 6week period. The PC served as an Internet web site and data server to provide on-line monitoring of sensor performance and live video images of the test bed. About 37 days of test bed data were remotely collected, downloaded, and analyzed. Hourly surface weather observations from MWO were separately collected. A custom set of data reduction and analysis tools were developed. The tools included a Fortran program developed to perform the bulk of the data reduction and analysis. The output of the program consists of continuous time series of sensor data and computed variables generated at ~10-s intervals. Hourly summaries of the data including mean and standard deviation values were also produced. The above data were also merged and compared with the surface weather observations. Figures are presented in this report to document and present the test bed setup, data, and analysis results.

This effort was considered primarily a demonstration and shakedown effort, as a number of assumptions and limitations were necessary and understood before the test bed installation. The most severe limitation on data collection and analysis resulted from problems encountered with obtaining and installing the video camera, and with the camera operation itself. Despite this and other difficulties encountered, a sufficient amount of useful data was successfully collected and analyzed to draw some conclusions on the adequacy of the test bed setup and the performance of the wind sensors. Results show several effects of snow and icing on wind sensor performance. One of the wind direction mechanical sensors failed early in the study due to heater-related bearing problems. The ultrasonic anemometer experienced a significant amount of data outages, and was unavailable 9 percent of the time. The failures are highly correlated to snow conditions. Other data suggests that the buildup of ice on the mast of the mechanical sensors is significant and affects the sensor performance. Several test bed setup and data collection recommendations are provided in support of a proposed larger scale effort.

1. INTRODUCTION.

The Weather Branch (ACT-320) of the Federal Aviation Administration (FAA) William J. Hughes Technical Center performed an informal field test and assessment of several anemometers located on Mt. Washington, New Hampshire, in February and March of 1999. The purpose of the effort was to perform a preliminary investigation of the severe weather performance capabilities of the anemometers currently used in the prototype Wind Hazard Information System (WHIS) at Juneau International Airport, AK, and the severe weather performance of other candidate wind sensors.

As background, this effort is part of a much broader feasibility study for the development and implementation of a prototype Wind Hazard Detection and Warning System for Juneau Airport in Juneau, Alaska. As envisioned, the end-state system would provide turbulence detection and warnings customized to the airport's challenging terrain. Mountains and rugged terrain around Juneau Airport restrict flight paths and can create complex and turbulent wind-flow patterns. To reduce the risk of aircraft encountering severe turbulence, the FAA currently requires that two major departure routes at Juneau be closed to Part 121 commercial aircraft whenever the centerfield and/or three anemometers on nearby mountains exceed FAA Operations Specifications for Part 121 air carrier operations in Juneau [1]. The WHIS, and the detection and warning system if implemented, will incorporate current guidelines in their respective Operations Specifications to maximize use of Juneau's turning-departure routes and support overall airport operational decisions.

Development of the WHIS is being conducted by the National Center for Atmospheric Research (NCAR), through the Turbulence Product Development Team (PDT) of the FAA Aviation Weather Research (AWR) program. Data gathering and analysis at Juneau is being performed by NCAR using a deployed array of sensors which include the centerfield and mountaintop anemometers currently employed in Part 121 Operations. The AWR Program is managed under AUA-430, which provides funding for and directs research related to weather phenomena affecting all phases of aviation. The purpose of the AWR program is to identify and develop weather-related science and technology which will improve safety as well as increase capacity. Funded activities range from basic research in various phenomena to prototype systems and products designed for both FAA and aviation industry users. The Weather Branch (ACT-320) is located at the Technical Center in Atlantic City, New Jersey, and provides continuous support to AUA-430 in this effort. The primary roles of ACT-320 include user needs assessments, conduct/oversight of demonstrations and evaluations, and meteorological assessments. Additional support in this effort includes requirements determination as well as engineering, and test and evaluation.

1.1 PURPOSE OF REPORT.

This report provides results of the test bed demonstration and preliminary assessment of sensor performance in support of selecting and maintaining wind sensors for the Juneau Airport prototype WHIS. The report documents the test bed setup, data collection, and analysis activities related to the demonstration and assessment.

1.2 SCOPE OF REPORT.

This report has been written and formatted in accordance with the FAA Test and Evaluation Process Guidelines [2]. The test guidelines have been tailored to account for this demonstration and assessment type activity. The body of this report contains a description of the test bed setup, sensors, test method, and data collection and analysis activities. Data analysis results and summaries are provided in the figures and appendix A at the end of this report. Discussion, conclusions, and recommendations based on results of the test bed and sensor performance are also provided. Detailed test bed data and plots are contained in appendices B and C and are provided as separate file attachments for electronic copies.

2. REFERENCE DOCUMENTS.

This section contains a list of all reference documents used in the development of this test report.

- 1. FAA Operations Specifications for Alaska Airlines Operations in Juneau, AK, C64, Effective 21 April 1998.
- 2. FAA Acquisition Management System (AMS) Test and Evaluation Process Guidelines, Content and Format of Operational Test (OT) Reports, appendix C-3, February 1999.
- 3. Mt. Washington Observatory, Home Page, http://www.mountwashington.org.
- 4. Mt. Washington and the Presidential Range Topographic Map, Scale 1:20,000, Appalachian Mountain Club, Boston, MA, ISBN 0-910146-97-7, Revised June 1989.
- 5. Handar Model 425 Series of Ultrasonic Wind Sensors, User's Guide, version 1.6, Sunnyvale, CA, July 1998.
- 6. Rosemount Model 871FA Ice Detector, Product Data Sheet 2239, Rosemount Inc., Minneapolis, MN, November 1977.
- 7. US Weather Net, Home Page, http://www.uswx.com/wx/us/nh/KMWN.

3. SYSTEM DESCRIPTION.

3.1 TEST SITE AND TEST BED LOCATION.

The test site is situated near the Mt. Washington Observatory [3], which is located on the summit of Mt. Washington in New Hampshire. The geographical summit has an elevation of 1917 meter (m) (6,288 feet) and is the highest point in the northeastern United States. The Observatory is a research facility which specializes in the conduct of scientific research and engineering test programs for the design, development, and testing of robust meteorological instrumentation. The most important feature of the facility is its unique location, which is subject to extremes of meteorological and climatic conditions equivalent to alpine and arctic zones such as Juneau, Alaska. The location and conditions provide the ideal natural test bed for assessing the severe weather performance of meteorological instrumentation. Snow and icing conditions are common on Mt. Washington from early fall through spring. The buildup of rime

ice on exposed surfaces is prevalent and often substantial. Based on the 43-year interval from 1935–78, the mean annual snowfall was 6.3 m (248 inches (in)). For some part of the day, the summit is in clouds or fog, at least 300 days out of the year. The lowest recorded temperature was -44°C (-47°F) and the mean hourly wind speed is 35.1 miles per hour (mph). Wind gusts exceeding 45 m·s⁻¹ (100 mph) are frequent in winter and early spring. The highest wind velocity ever recorded anywhere in the world was 103 meters per second (m·s⁻¹) (231 mph) which was measured at the Observatory.

The sensor test bed location is approximately 340 m (1125 feet) and 9° north of the summit. It is on the north slope, and about 67 m (220 feet) below the summit. As a result, it has excellent exposure for winds from all directions, especially for the large northwest sector extending southwest through northeast. A topographic map [4] showing the location of the test bed with respect to the summit and Mt. Washington Observatory is shown in figure 1.

3.2 SENSORS.

The array of four mechanical wind sensors and an ultrasonic anemometer were mounted at a height of 2.6 m (8.6 feet) above ground on a ~13.7 m (45-foot (ft)) horizontal steel I-beam oriented in a generally northeast/southwest direction. Supplementary weather instrumentation and equipment included a temperature and relative humidity probe, an ice detection sensor, a video camera, a datalogger, a personal computer (PC), and various communications equipment. Electrical power and data communications were supplied from a heated instrument shelter located ~30 m (100 feet) southeast from the sensors. Schematic diagrams showing elevation and plan views of the test bed setup and instrumentation are shown in figures 2 and 3, respectively. Photographs of the test bed and sensors are shown from varying views in figures 4 and 5. The photographs in figure 6 show views of the test bed with respect to the Observatory.

Two pairs of Hydro-Tech mechanical wind sensors manufactured by Taylor Scientific Engineering were installed. Each pair consisted of an individual Model WS-3 Heated Rotor Anemometer and a separate Model WD-3 Heated Direction Vane. The sensors are particularly designed for rugged applications and are electrically heated and temperature controlled. Each has a 2000-watt (W) heater, which is approximately 33 percent more than the standard production models currently in use in Juneau, AK. Photographs of the rotor anemometer and the direction vane are shown in figure 7.

A modified Handar Model 425AH ultrasonic anemometer was also installed for testing. Production units of the 425AH have thermostatically controlled transducer heads with a total heat output of about 30 W. The modified unit, as shown in figure 8, has additional heating elements covering the sensor body and transducer arms, and consumes approximately 240 W. The sensor was mounted without the bird spikes installed. It has an integrated microprocessor that acquires and processes wind data, and performs serial data communications. The array of three equally spaced ultrasonic transducers in a horizontal plane measures the transit time for sound to travel from one transducer to another. The transit time depends on the wind velocity along the sonic path. Unreliable readings, which may occur when large raindrops or ice pellets hit a transducer, are eliminated by an internal signal processing technique [5]. The version of firmware used in the unit tested was version 2.03.

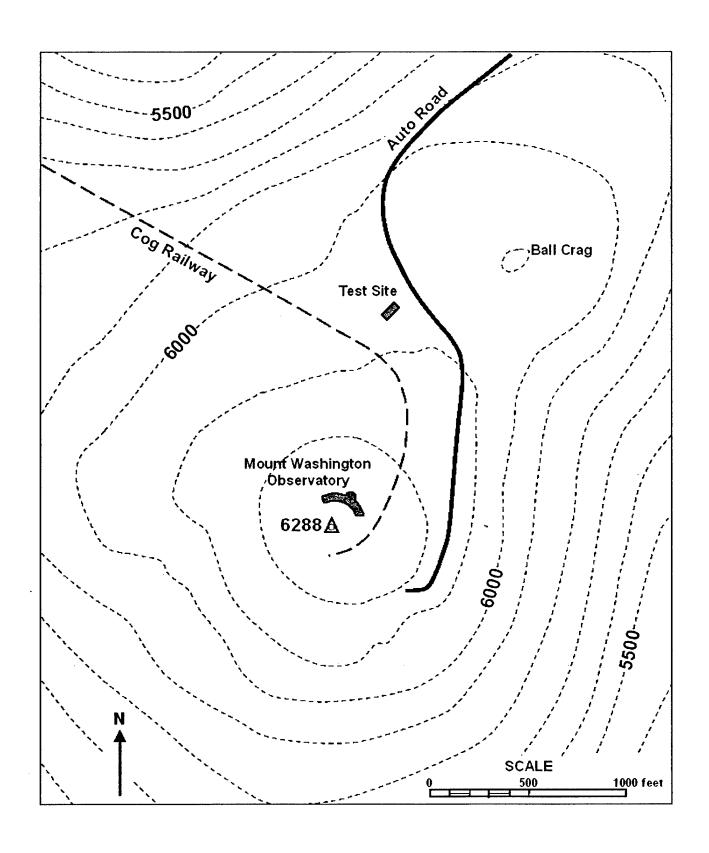


FIGURE 1. SITE MAP WITH TEST SITE

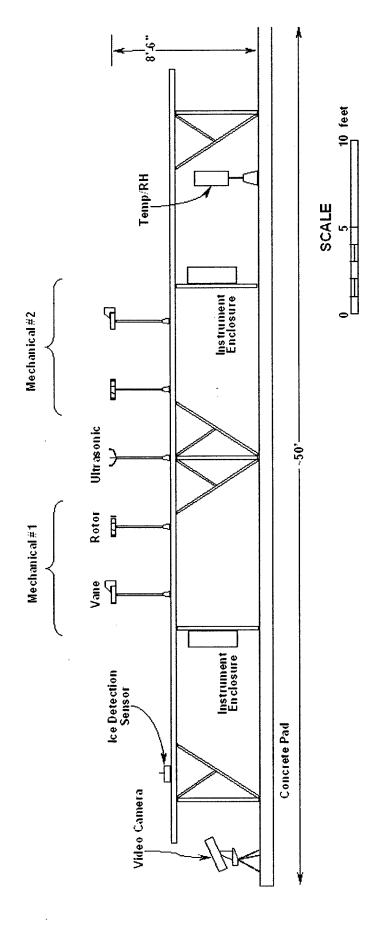


FIGURE 2. SCHEMATIC ELEVATION VIEW OF TEST BED AND SENSORS

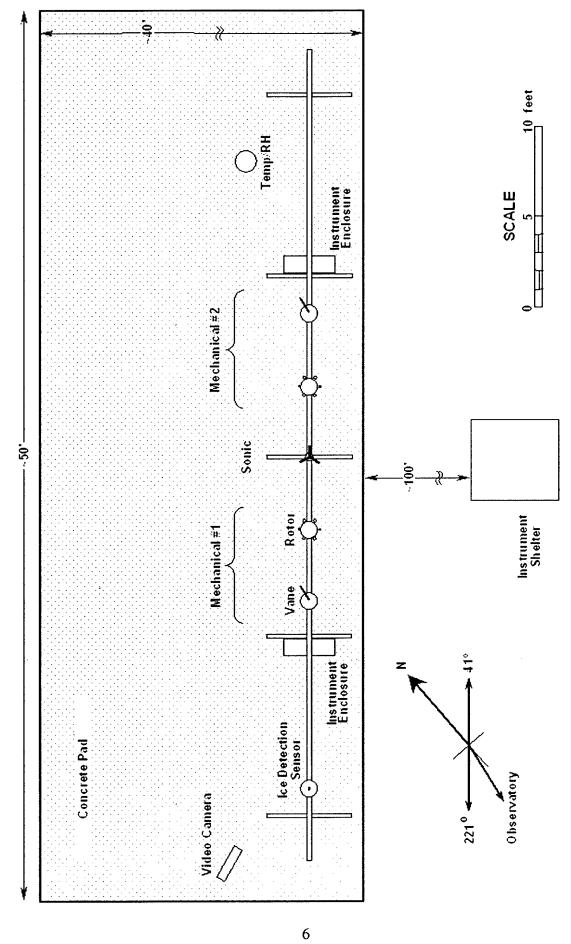
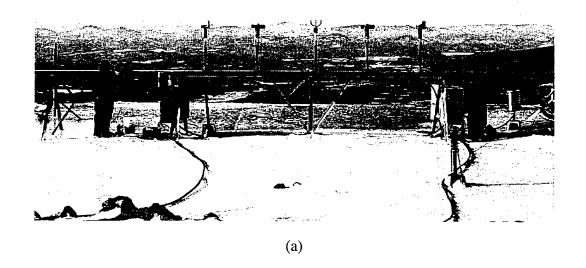


FIGURE 3. SCHEMATIC PLAN VIEW OF TEST BED AND SENSORS



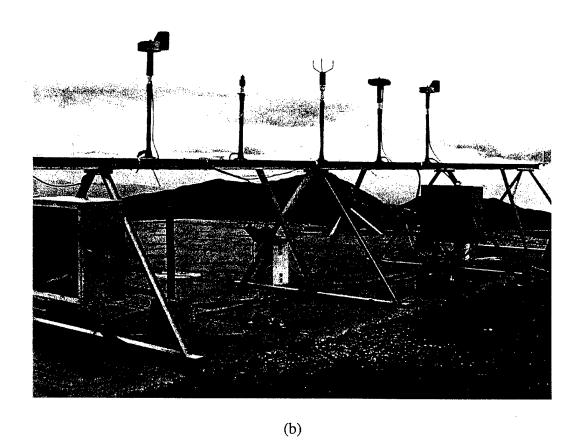
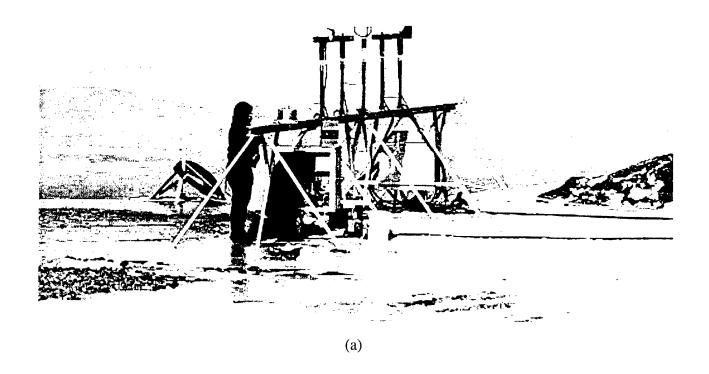


FIGURE 4. VIEWS OF SENSORS LOOKING NORTHWEST (a), AND NORTH (b)



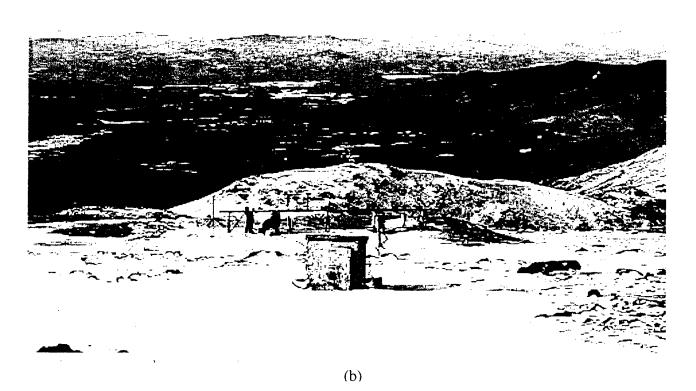
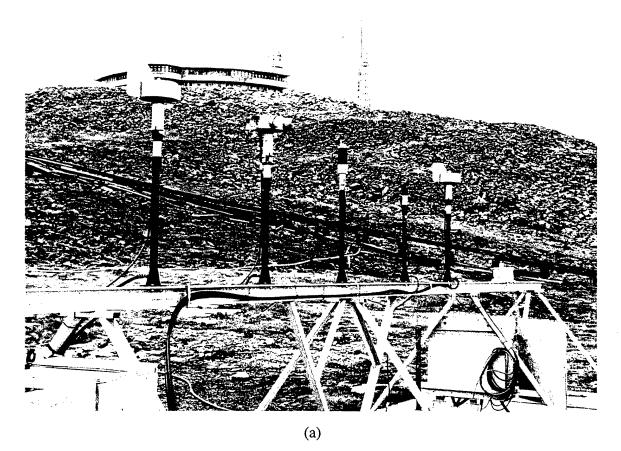


FIGURE 5. VIEW OF SENSORS LOOKING NORTH (a), AND TEST BED AND SHELTER LOOKING NORTHWEST (b)



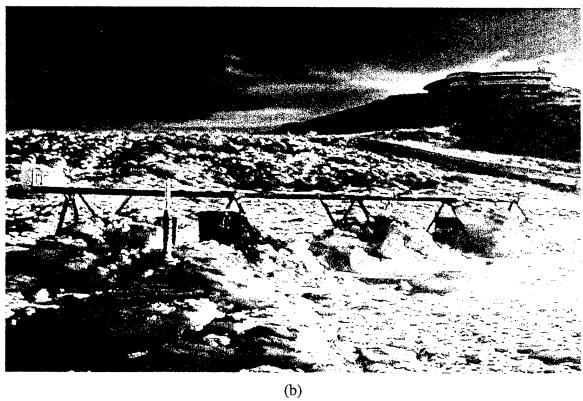


FIGURE 6. VIEWS OF THE TEST BED AND OBSERVATORY (a), AND TEST BED IN SNOW CONDITIONS (b)





FIGURE 7. MECHANICAL WIND SENSOR ROTOR (a), AND DIRECTION VANE (b)

(b)

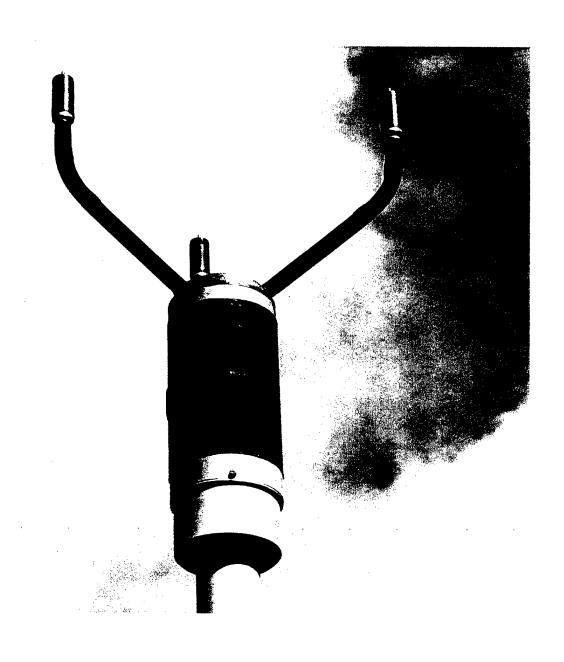


FIGURE 8. ULTRASONIC ANEMOMETER

3.3 OTHER INSTRUMENTS.

To provide an automated means of detecting icing conditions, a Rosemount Model 871FA Ice Detector [6] was installed at the test site. Because the sensor is designed for installation through the skin of an aircraft, a special metal housing was fabricated to mount and protect the sensor body. A photograph of the sensor and the housing is shown in figure 9. The sensor measures the amount of ice mass accumulation on a cylindrical metal probe. The probe is vibrated at a natural resonance frequency of 40 kilohertz (kHz). As ice accretes, the frequency of the vibration decreases. Once a preset amount of ice mass has accumulated, the cylinder heater is activated to melt and remove the ice. A nominal time history of the probe output voltage based on its operating principles is shown in figure 10. The figure shows the voltage increasing with ice accumulation, and then dropping to its threshold value as the heater is activated to remove the ice. The standard trip point is 0.5 millimeter (mm) (0.020 in) ice thickness with an accuracy of about ±25 percent.

Air temperature and relative humidity were measured by a Campbell Scientific HMP45C integrated temperature and relative humidity probe manufactured by Vaisala, Inc. The probe consists of a platinum resistance thermometer and capacitive-type relative humidity sensor housed directly in a 12-plate Gill solar radiation shield. The temperature measurement range and accuracy is −39 to +60°C, and <±0.5°C, respectively. Relative humidity field accuracy at 20°C is ≤±3 percent over the full RH range of 0−100 percent. To prevent the buildup of snow and ice directly on the sensor, the unit was mounted in a specially fabricated aluminum canister with top and bottom ventilation. The open bottom of the canister was situated about 0.5 m (1.5 feet) above ground. A photograph of the enclosure is shown in figure 11.

A Pelco PT780 series panning and tilting video camera with preset positioning capabilities was set up to provide real-time visual monitoring and recording of the rime icing on the sensors. The camera enclosure has a heater and pressurized dry nitrogen system to prevent icing and condensation buildup on the camera lens. The camera was connected via unshielded coaxial cable to the LRD41C video receiver and drive controller unit located in the instrument shelter. A photograph of the video camera is shown in figure 12. Unfortunately, difficulties were encountered with acquiring and installing the camera which severely limited its usefulness for the data collection effort. The camera was received from the manufacturer in damaged condition and was not available for testing and burn-in prior to the installation on Mt. Washington. In addition, the test bed camera mount, which was to be manufactured by Mt. Washington personnel, was not complete at the time of installation of the other equipment. Difficulties in coordinating a subsequent installation of the camera by Observatory personnel further delayed use of the camera. When the camera was finally installed by Observatory personnel, the lenses became fogged, rendering the video useless. The fogging should not have occurred since the camera was supposedly pressurized with dry nitrogen. As a result of the numerous problems encountered, video images of the test bed and sensors were not available. This proved to be the most serious setback in data collection, because it prevented correlation of sensor performance with a real-time assessment of weather conditions.

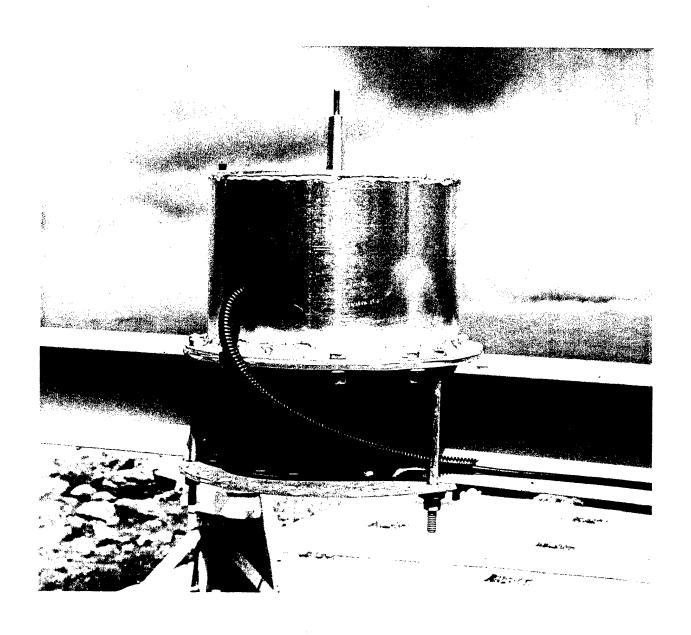


FIGURE 9. ICE DETECTION SENSOR

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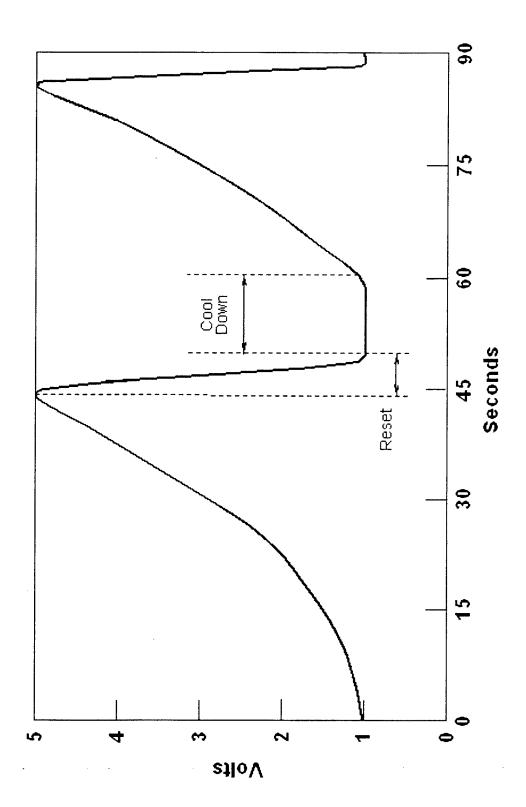


FIGURE 10. NOMINAL ICE DETECTION SENSOR RESPONSE

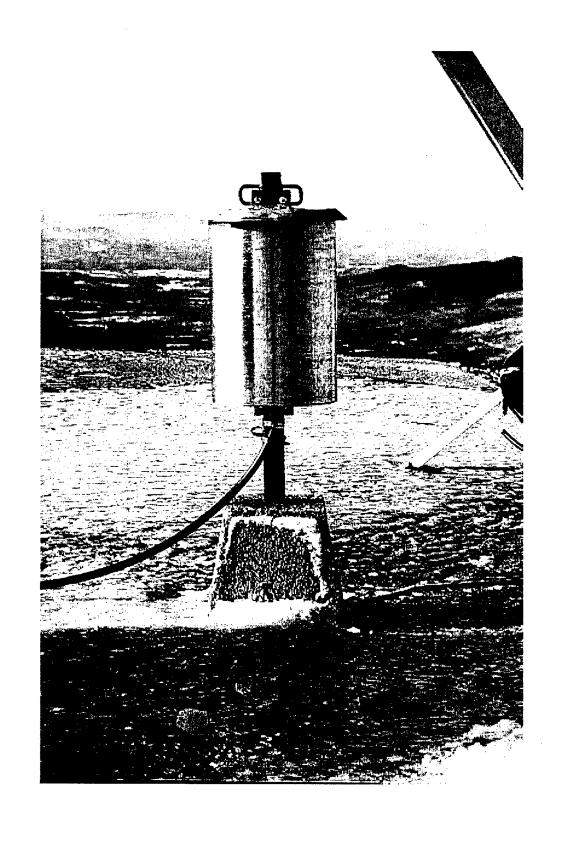


FIGURE 11. TEMPERATURE AND RELATIVE HUMIDITY ENCLOSURE

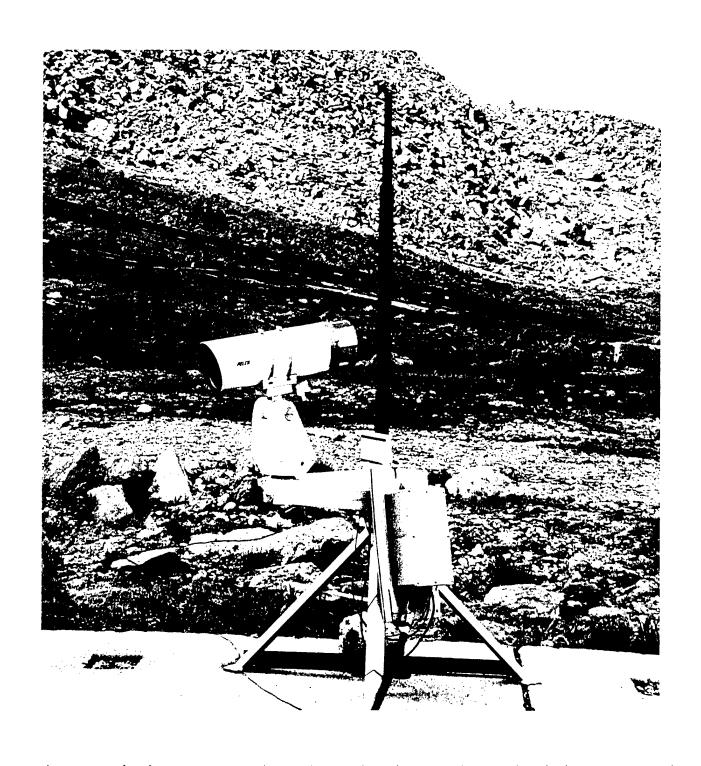


FIGURE 12. VIDEO CAMERA

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3.4 DATA ACQUISITION.

The test bed was designed and set up for complete unattended operation and maintenance during the test period. Data acquisition from the weather sensors was accomplished either directly, or via a Campbell Scientific Model CR23X Micrologger which was located in the environmental enclosure on the instrument-mounting fixture. Photographs of the two environmental enclosures are provided in figure 13. The datalogger supplied data to a Windows NT-based PC located in the heated shelter. The nominal sampling and recording rates for the ultrasonic sensor and the balance of other sensors were 1 and 10 seconds (s), respectively.

A block diagram showing data collection is furnished in figure 14. The PC performed the data recording, and was connected to the Observatory via a 10 BaseT connection using Internet Protocol. The test bed PC was assigned an Internet Protocol (IP) address, and set up as an Internet web and File Transfer Protocol (FTP) server to facilitate remote monitoring, control, and collection of test bed data. The test bed web server also supplied live video camera images and on-line analysis tools in order to provide continuous monitoring and evaluation of sensor data. Pictures of the web site with on-line analysis and camera frame features are shown in figures 15 and 16.

4. TEST AND EVALUATION DESCRIPTION.

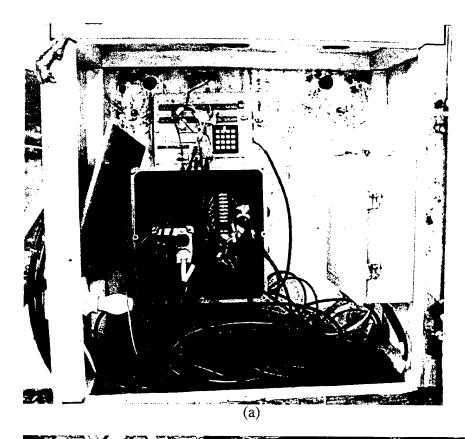
4.1 TEST OBJECTIVES/CRITERIA.

The objective of the study was to evaluate the effects of icing and snow on the performance of the wind sensors. A secondary objective was to design and develop an unattended sensor test bed for use in future tests on Mt. Washington.

4.2 TESTING DESCRIPTION.

Original plans called for testing over a 3-month period, but difficulties with the data collection suite limited the period of useful data collection. Consequently, the evaluation consisted of a single 6-week activity for assessing wind sensor performance. No particular subtests were performed or critical test issues considered. Test bed setup and installation of the sensors and instrumentation took place on Mt. Washington the week of February 8, 1999, under unfavorable weather conditions. Initial data collection began on February 12, 1999, with full data collection taking place from February 19, 1999, to the end of the effort on March 21, 1999. The test bed was dismantled on June 17, 1999.

Sensors utilized in the test were installed as received from the manufacturers and other organizations. Special mounting enclosures were designed and fabricated for the ice detection sensor and the temperature and relative humidity probe. No specific calibration procedures were performed, and the azimuth alignment of the wind sensors was estimated by means of a compass and visual inspection. As previously mentioned, the deployment of the camera was plagued with numerous difficulties, and very little useful video data was acquired. The test bed data was monitored remotely and by ACT-320 at the Technical Center. Data transfer was accomplished



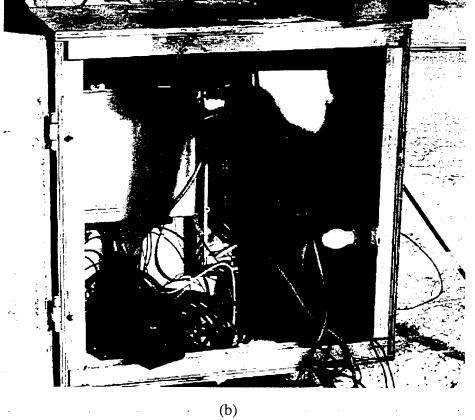


FIGURE 13. DATALOGGER INSTRUMENT ENCLOSURE (a), AND OTHER INSTRUMENT ENCLOSURE (b)

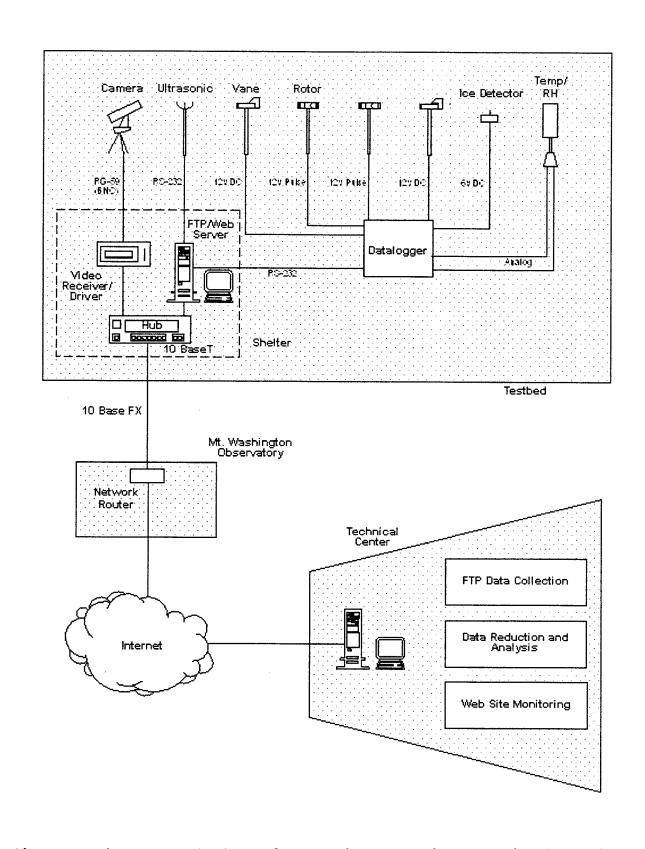


FIGURE 14. DATA COLLECTION AND PROCESSING BLOCK DIAGRAM

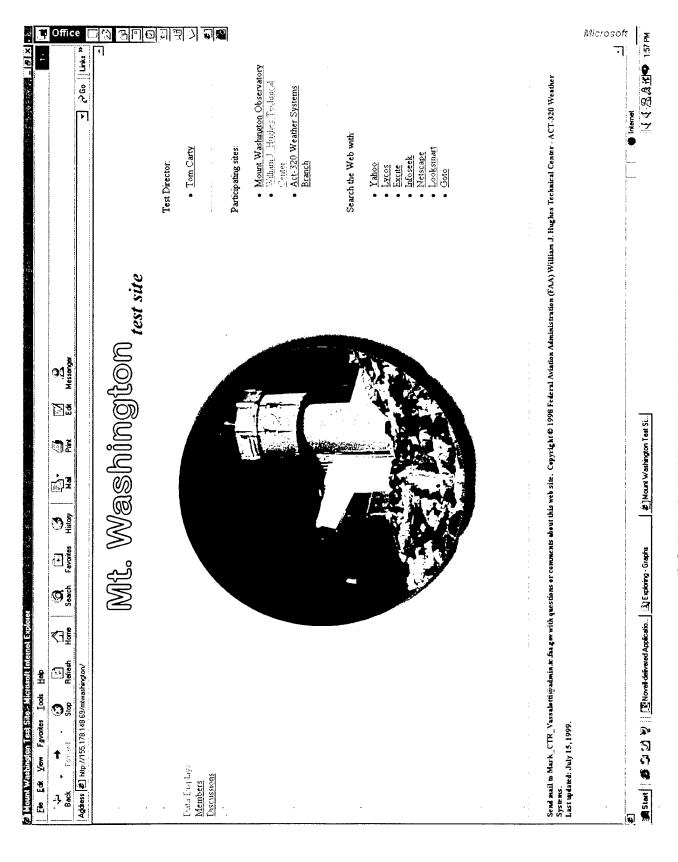


FIGURE 15. TEST SITE MAIN WEB PAGE

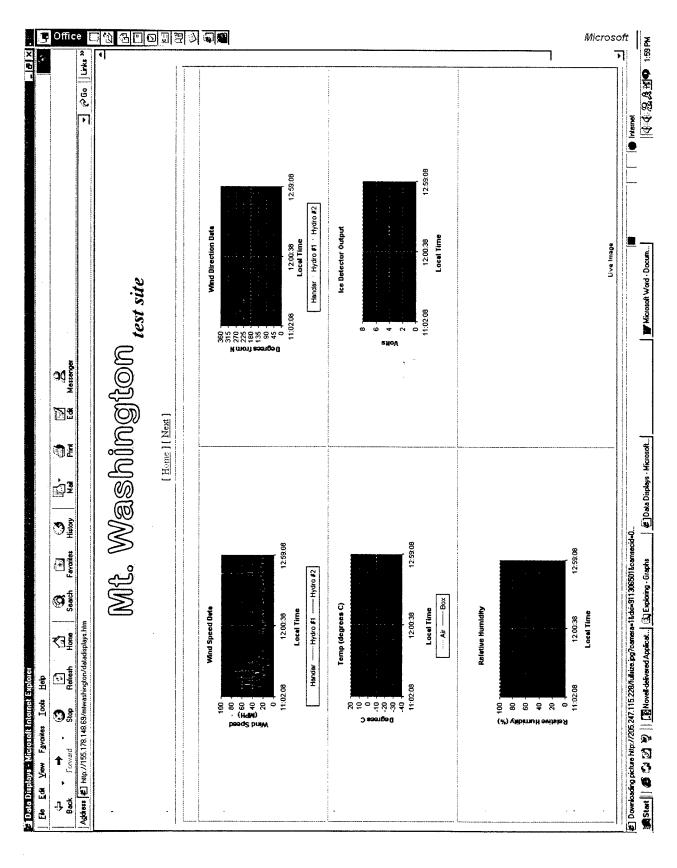


FIGURE 16. TEST SITE SENSOR DISPLAY WEB PAGE

via the Internet by accessing the test bed server and on-line data analysis tool. Data files were downloaded on a daily basis for later data reduction and analysis.

4.3 DATA COLLECTION AND ANALYSIS METHOD.

4.3.1 Data Recording.

Data collection was performed continuously with two data files being created and stored for each day. Data files were remotely retrieved from the test bed on a daily basis via the Internet using FTP. Approximately 37 days of test bed data were collected. Each day of data is comprised of two separate files. One file consists of the mechanical wind sensor data along with the other meteorological data, and the other file consists of the sonic anemometer data. The formats of these source files are provided in figures 17 and 18, respectively. In addition to the test bed data, hourly Aviation Routine Weather Report (METARs) routinely reported by the Observatory were separately collected through an archive source [7] via the Internet.

4.3.2 Data Reduction.

All recorded data was remotely downloaded to the Technical Center for analysis. A custom set of Digital Visual Fortran 95 software routines were developed to perform the bulk of the test bed data reduction and analysis. The programs perform full data decoding, and implement a variety of data quality analysis and normalization routines. Several conventional meteorological wind conversion and rectification techniques were also incorporated. Two types of output are provided by the program. The first is hourly mean and standard deviation values of the observed and computed weather parameters, along with a collection of corresponding hourly surface observations from the Observatory. A sample of the hourly summaries and weather observations is shown in figure 19. The second type of output from the program is a time series of ~10-s averaged observed and computed weather data. A sample of this output is shown in figure 20. The legend for figures 19 and 20 is furnished in figure 21. Output from the program along with the hourly weather observations were merged and imported into Microsoft Excel 97 spreadsheets to facilitate plotting. A sample worksheet is shown in figure 22.

4.3.3 Data Visualization.

Final data visualization, analyses, and interpretation were accomplished using graphical and plotting routines provided in Excel. Two plots were created for each day of data. Samples of the plots are provided in figures 23 and 24. The first plot shows the wind speeds and additional weather data from the test bed and hourly surface observations. The rotor, sonic, and observed wind speed and gust speeds are shown on the primary ordinate axis. Wind data from the Number 1 set of mechanical sensors is not shown because heater failures which occurred during installation of the rotor sensor prevented the use of its associated direction vane. Wind speeds from the sonic sensor are plotted over the rotor wind speeds. For reference, a red-dashed horizontal baseline is used to visually depict a 35-knot (kn) wind threshold, which is one of the wind speed restrictions under the current Juneau Operations Specification, depending on the particular aircraft flight path and mountain wind conditions. Values of temperatures and visibility, and normalized values of the icing sensor and relative humidity in percent, are plotted

08:35:42,42,259.8,.3,42,237.8,.485,5.211,85.5,1.228,10.93

Field	1	2	3	4	.5	6	7	8	9	10	11
Example	08:35:42	42	259.8	.3	42	237.8	.485	5.211	85.5	1.228	10.93
Descrip tion	DAS Time	Mechan: Speed	ical #1	Rsrved	ı	ical #2	Rsrved	Temp	RH (perce	Ice (V)	DAS Temp
		(MPH)	Dir		(MPH)	Dir		(0)	nt)	()	(C)

File:

```
08:35:42,42,259.8,.3,42,237.8,.485,5.211,85.5,1.228,10.93
08:35:52,44,244.1,.455,44,249.9,.416,5.214,85.5,1.225,10.93
08:39:31,43,240.9,.472,43,239.4,.48,5.404,84.4,1.211,10.98
08:39:41,44,233.8,.496,44,242.3,.466,5.407,84.3,1.22,10.98
08:39:51,41,235.3,.492,41,242,.468,5.414,84.3,1.235,10.99
08:40:01,44,271.1,0,42,261.2,.278,5.42,84.2,1.229,10.99
08:40:11,43,222.8,.504,43,252.3,.394,5.424,84.3,1.23,11
08:40:21,42,253.5,.383,41,231.7,.5,5.42,84.4,1.217,11
08:40:31,51,255.8,.355,50,233.4,.496,5.43,84.9,1.204,11
08:40:41,47,267,.157,48,249.2,.422,5.436,85.2,1.217,11
08:40:51,50,246.6,.441,49,221.7,.503,5.45,85,1.208,11.01
08:41:01,50,257.9,.327,51,264.2,.221,5.453,85,1.212,11.01
08:41:11,44,264.4,.217,44,252.3,.393,5.469,84.7,1.209,11.01
08:41:21,41,251.1,.405,40,241.3,.471,5.469,84.4,1.215,11.01
08:41:31,39,277.8,0,38,246.7,.441,5.486,84.2,1.202,11.02
08:41:41,38,266.3,.172,37,263.4,.237,5.489,84.2,1.214,11.02
08:41:51,40,260.6,.287,40,250.1,.414,5.495,84.3,1.196,11.02
08:42:01,41,253.1,.385,41,246.7,.44,5.492,84.4,1.199,11.03
08:42:11,47,253.5,.382,47,246.7,.441,5.509,84.6,1.191,11.03
08:42:21,46,241.5,.469,45,254.7,.368,5.518,84.5,1.196,11.03
```

FIGURE 17. DATALOGGER FILE FORMAT

08:35:36° W1P2480018.5MEF~

Field	1	2	3	4	5	6	7	8	9
example	08:35:36	^	W1	P	248	0018.5	M	EF	~
Description	Time	02h (STX)	1-s ave indicator	Sensor 'Pass' flag	Dir	Speed	mph	Checksum	03h (ETX)

File: 17:02:51^W1P0110026.1MDE~ 17:02:53°W1P0140028.7ME9~ 17:02:57 W1P0110027.6ME4~ 17:02:59 W1P0110027.6ME4~ 17:03:00°W1P0120028.5ME5° 17:03:02 W1P0120028.5ME5~ 17:03:03:03:04:0120028.5ME5~ 17:07:05 V1P0110029.9ME9 :097W1P0110039 9ME9 17:03 17:03:10^W1P0110029.9ME9 Time delta > 1 second 17:03:12^W1P0120028.2ME2^ 17:03:13 W1P0120028.2ME2 17:03:15^W1P0120028.2ME2~ 17:03:16^W1P0100027.0MDD~ 17:03:21 W1P0100027.0MDD~ 17:03:22 W1P0100027.0MDD~ 17:03:23^W1P0070027.2ME5~ 17:03:25 W1P0070027.2ME5~ 17:03:26^W1P0190030.9ME9~ 17:03:28^W1P0190030.9ME9~ 17:03:32 W1P0150027.1ME3~ 17:03:34 W1P0150027.1ME3~ 17:03:35 WIP0150027.1ME3~ `W. 110033.1MDC~ 17:03:3 W1P0110033.1MDC Extra STX character 17:03:40 W1P0100029.8ME7 17:03:44°W1P0140035.5ME5~ 17:03:46^W1P0200029.4ME4~ 17:03:47 W1P0200029.4ME4~ 17:03:49 W1P0200029.4ME4~ 17:03:50°W1P0140035.1ME1 17:03:52 W1P0140035.1ME1 17:03:53°W1P0140035.1ME1 17:03:58°W1F9990999.9N08 17:03:59 \ 11F9990999.9M 17:04:01^W1P0180032.3ME4^ Sensor failure flags 17:04:02^W1P0180032.3ME4~ 17:04:04^W1P0150031.5ME2~

FIGURE 18. ULTRASONIC FILE FORMAT

Mt. Washington Data

	9	M14 RMK
DATE = 0316	2 3 4 5	2359 1604592 31066G78KT 0SM -SN BLSN FZFG VV000 M14/M14 RWK LGT LCG 0055 1605552 31070G83KT 0SM BLSN FZFG VV000 M15/M15 RWK SNE35 LGT LCG 0159 1606592 31070G83KT 0SM BLSN FZFG VV000 M15/M15 RWK PK WND 310103/45 0259 1607592 32070G93KT 0SM BLSN FZFG VV000 M16/M16 RWK PK WND 310106/10 0353 160852 32081G109KT 0SM BLSN FZFG VV000 M16/M16 RWK PK WND 310106/10 0559 1610572 32076G109KT 0SM BLSN FZFG VV000 M18/M18 RWK LGT LCG 0557 1610572 32076G105KT 0SM BLSN FZFG VV000 M18/M18 RWK PK WND 320104/22 0557 1610572 32076G105KT 0SM BLSN FZFG VV000 M18/M18 RWK PK WND 320104/22 0557 1612472 32076G105KT 0SM BLSN FZFG VV000 M18/M18 RWK PK WND 320108/ZEG 1058 1613582 29070G82KT 0SM BLSN FZFG VV000 M16/M16 RWK FZFG INTWT SCOPEN OFFI 1159 1616592 29070G82KT 0SM BLSN FZFG VV000 M16/M16 RWK FZFG INTWT SCOPEN OFFI 1159 1616592 29076G82KT 0SM BLSN FZFG VV000 M16/M16 RWK FZFG INTWT FZFG LGT LCG 1155 1615582 29076G88KT 1/16SM BLSN FZFG VV000 M16/M16 RWK FZFG INTWT FZFG LGT 1CG 1155 161552 29076G88KT 1/16SM BLSN FZFG VV000 M16/M16 RWK FZFG LGT LCG 1155 161552 28076G98KT 1/16SM BLSN FEWOU M12/M17 RWK GIT LCG 1165 1620512 28071G83KT 0SM DRSN FEWOU M12/M15 RWK CIG LMG RPDLY 1/16S 1620512 28071G83KT 0SM DRSN FEWOU M12/M15 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FEWOU M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FEWOU M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 162052 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 1620502 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 1620502 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 1620502 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWK LGT LCG 1165 1620502 28071G83KT 0SM DRSN FZFG VV000 M12/M12 RWG LGT LCG 1165 16205

9 10		11 12	12	13		14	15	16	17	18	119	20
00-01 1 (99.9)	1 (9	(6.6	86	326 41	0	326 16 10 2	318 60	0 -16 12 2	16 -60	7 -44	-13	06
01-02 131	1 (8.	(83.6)	86	330 16	0	327 21 13 2	321 58 5 9	2 -21 12 2	10 -58 13 9	8 -37 10 8	-13	06
02-03 186 (72.4)	6 (7;	2.4)	97 11	330 35	0	329 20 21 3	322 57 8 11	1 -20 16 3	11 -57 16 11	8 -37 11 10	-14	06
03-04	,4	(43.7)	56 47	331 18	0	324 26 16 2	321 61 6 10	7 -26 16 2	10 -61 17 10	2 -35 13 9	-14	8
04-05 285	5 (4,	(44.8)	98	329 26	0	311 30 13 5	320 61 7 10	18 -30 16 5	10 -61 19 10	-9 -31 10 9	-15	68
05-06 266 (53.4)	· 2		98	346 52	0	316 33 16 2	316 78 35 53	29 -33 31 2	28 -78 45 53	0 -45 36 53	-16	88

FIGURE 19. SUMMARY FILE FORMAT

6	13		15	4	1,	5		9			1	8	19	20	12
= 02	,	u	·	r	~	_		1		d	1		*	_	0
0:00:1	26.5	15.9	24.6	22.7	37.4	24.2	. t	-6.7	-10.9) M	-12.8	-1.5	-11.1	90.0	9.00 9.00
0:00:2	9.6	N	9		ا	0	9	. 6		5	9		; ; ;	0	. &
0:00:3	1.2	2	ω.	ω.	2	9	٠	9	10.	ω.	ä		÷	0	8
0:00:4	2.2	4		7.	4.	φ.	Η.	ъ.	2	9	•	0	÷.	0	8
0:00:5	1.7	۲.	7.	7.	0	0	4.	9	Ή.	ω.	7.	•	11.	0	ω.
0:01:0	4.0	т		ο	щ	0	9	5.	ö	7.	Ŋ.	ä	H.	。	8
0:01:1	8.6	2	9	ω	2	6	•	9	2	•	•	•	Ĥ.	0	ω.
0:01:2	5.0	т М	7.	9.	9	0	7	9	رى	7.	8	$\vec{\vdash}$	Ξ.	0	8
0:01:3	0.1	ж	2,	ο	2	ω.	Ω.	5.	2	5.	9.	•	Η.	0	φ.
0:01:4	9.8	4.	ω.	0	7.	ω,	•	5	0	4.	4.	•	Η.	0	8
0:01:5	8.8	4.	÷	9	5	ω.	7.	5	7.	4.	4.	•	Η.	0	φ.
0:02:0	1.8	2	7	7.	ä	9	•	δ.		4.	19.	٠	11.	0	8
0:02:1	7.1	2	7.	7.	5.	9.	6	5		7.	ω.	•	11.	0	ω.
0:02:2	1.0	3	7.	9.	9	φ.	9	Ŋ.		5	φ.	•	Η.	0	ω,
0:02:3	6.3	3	6	7.	9	7.	9	4.		4.	0	•	Η.	0	φ.
0:02:4	8.0	2	4.	7.	3	۲.	•	4.		4.	ω	•	11.	0	ω
0:02:5	4.8	0	9	5	φ.	5	&	4.	•	4.	7		11.	0	ω
0:03:0	6.0	∺	9.	7.	÷	9.	ä	5.		7.	$\ddot{\vdash}$	•	ä	。	ω
0:03:1	9.5	2	œ	7	υ. •	7.	ä	δ.		δ.	ω,	•	÷.	。	ω
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0:03:4	7.6	4	÷	。	0	ij	9	5.		9	9.	•	ij	0	ω
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0:04:0	8.1	· 6	ъ.	7	7.	2	7.	9	φ.	9	2	•	ij	0	ω
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0:04:2	5.0	4.	9.	。	Ŋ.	Ţ.	٠	9	•	9	5	٠	$\ddot{-}$	0	ω.
0:04:3	7.3	υ.	· 0	ά.	7.	2	٠	7.	0	7.	Η.	•	i.	ö	œ
0:04:4	4.6	δ.	。	0	9	0.	3	4.	•	4.	5.	•	Η.	ö	ω,
0:04:5	4.8	2	9.	7.	ζ.	5.	ъ.	•	•	2	7.	•	ä	0	œ
0:05:0	6.7	9.	÷.	4.	Ŋ.	4.	4.	4.	•	4.	•	•	Ή.	$\dot{\circ}$	ω,
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0:05:3	4.	0	7	5	0	9	7.	•	•	ė.	7	•	÷	0	ω
0:05:4	7.	ა	7	5	ω.	Š.	4.	•	5.	ė.	•	•	÷	0	œ
0:05:5	ъ.	•	7	7.	。	7.	•	•	•		•	•	ä	ö	œ

FIGURE 20. OUTPUT FILE FORMAT

Note	Group	Description
1	File	Date (mmdd)
2		Time Converted (LST)
3		Day of month and time in UTC (ddhhmm)
4	METAR	Wind direction, speed, and gust (true north, knots)
5		Visibility, present weather, sky conditions, temperatures
6		Remarks, including icing information (bold)
7		Mean Values
8		Standard Deviation Values
9		Analysis period (hour LST)
10		Sample size, N (sample sizes less than 300 are not shown)
11		Sonic Failure Rate (percent)
12		Normalized Icing (percent)
13		Mechanical #1 direction and speed
14	Test bed	Mechanical #2 direction and speed
15	Test bed	Sonic direction and speed
16		(Mechanical #1 - Mechanical #2) direction and speed difference
17		(Mechanical #1 - Sonic) direction and speed difference
18		(Mechanical #2 - Sonic) direction and speed difference
19		Temperature (°C)
20		Relative Humidity (percent)

FIGURE 21. LEGEND TO SUMMARY AND OUTPUT FILE FORMATS

NWS Gust	Vis	××	Cloud	Temp Re	Remarks 1	Hydro1 Hydro1 Dir Spd	Hydro1 I Spd	Hydro2 Hydro2 Handar Handar Dir Spd Dir Spd	tydro2 F Spd	landar H Dir		H1-H2 Dir	H1-H2 Spd	H1-H2 O <u>i</u> r	H1-H2 Spd	H2-Han H2-Han Dir Spd	H2-Han Spd	Temp	풒
25	1/16SM 3L	LSN FZF	VV000 I	1/16SM 3LSN FZF VV000 M16/M162FG INTMT	3 INTMIT	173.3	0	315.2	50.9	0	0	-141.9	-50.9	0	0	0	0	-14.8	88.1
						173.3	0	314.2	52.7	0	0	-140.9	-52.7	0	0	0	0	-14.8	88
						173.3	0	315.3	51.5	0	0	-142	-51.5	0	0	0	0	-14.8	88.1
						173.3	0	324	51.5	0	0	-150.7	-51.5	0	0	0	0	-14.8	88.1
						173.3		301.7	55.2	0	0	-128.4	-55.2	0	0	0	0	-14.8	88
						173.3	0	316.8	50.3	0		-143.5	-50.3	0	0	0	0	-14.8	88
						173.3	0	320.7	43.5	0	0	-147.4	-43.5	0	0	0	0	-14.8	88
						173.3	0	326.7	42.3	0	0	-153.4	-42.3	0	0	0	0	-14.8	88
						173.3	0	326.7	41.7	0		-153.4	-41.7	0	0	0	0	-14.8	88
						173.3	0	322.5	44.7	0	0	-149.2	-44.7	0	0	0	0	-14.8	88
						173.3	0	320.9	42.3	0		-147.6	-42.3	0	0	0	0	-14.8	88
						173.3	0	327.6	42.9	0	0	-154.3	-42.9	0	0	0	0	-14.8	88
						173.3	0	322	44.7	0	0	-148.7	-44.7	0	0	0	0	-14.8	88
						173.3	0	315	37.4	0	0	-141.7	-37.4	0	0	0	0	-14.8	88
						173.3	0	337.3	39.8	0	0	-164	-39.8	0	0	0	0	-14.8	88
						173.3	0	7.5	46.6	0	0	165.8	-46.6	0	0	0	0	-14.8	88
						173.3	0	339.9	39.8	0	0	-166.6	-39.8	0	0	0	0	-14.8	88
						173.3	0	336.5	42.3	0	0	-163.2	-42.3	0	0	0	0	-14.8	88
						173.3	0	326.5	41.1	0	0	-153.2	-41.1	0	0	0	0	-14.8	88
						173.3	0	334.5	45.4	0	0	-161.2	-45.4	0	0	0	0	-14.8	88
						173.3	0	341.5	46	0		-168.2	-46	0	0	0	0	-14.8	88
						173.3	0	330.1	50.9	0		-156.8	-50.9	0	0	0	0	-14.8	88
						173.3	0	312.7	42.9	0		-139.4	-42.9	0	0	0	0	-14.8	88
						173.3	0	304.8	37.4	0		-131.5	-37.4	0	0	0	0	-14.8	88
						173.3	0	335	43.5	0		-161.7	-43.5	0	0	0	0	-14.8	88
						173.3	0	334.5	43.5	0		-161.2	-43.5	0	0	0	0	-14.8	88
						173.3	0	332.1	38.6	0		-158.8	-38.6	0	0	0	0	-14.8	88
						173.3	0	335.7	49	0		-162.4	-49	0	0	0	0	-14.8	88
						173.3	0	322.7	46	0		-149.4	-46	0	0	0	0	-14.8	88
						173.3	0	331.5	46	0		-158.2	-46	0	0	0	0	-14.8	88
						173.3	0	328.9	48.4	0		-155.6	-48.4	0	0	0	0	-14.8	88
						173.3	0	350.1	49	0		-176.8	-49	0	0	0	0	-14.8	88
						173.3	0	327.7	44.1	0		-154.4	-44.1	0	0	0	0	-14.8	88
						173.3	0	330.1	47.8	0	0	-156.8	-47.8	0	0	0	0	-14.8	88
						173.3	0	325.8	49	0	0	-152.5	-49	0	0	0	0	-14.8	88
						173.3	0	325.4	46	0	0	-152.1	-46	0	0	0	0	-14.8	88
						173.3	0	322.2	48.4	0		-148.9	-48.4	0	0	0	0	-14.8	88
						173.3	0	328.1	49.7	0		-154.8	-49.7	0	0	0	0	-14.8	88
						173.3	0		55.2	0	0	-154.3	-55.2	0	0	0	0	-14.8	88
						173.3	0		53.3	0		-151.5	-53.3	0	0	0	0	-14.8	88
						1700	,												

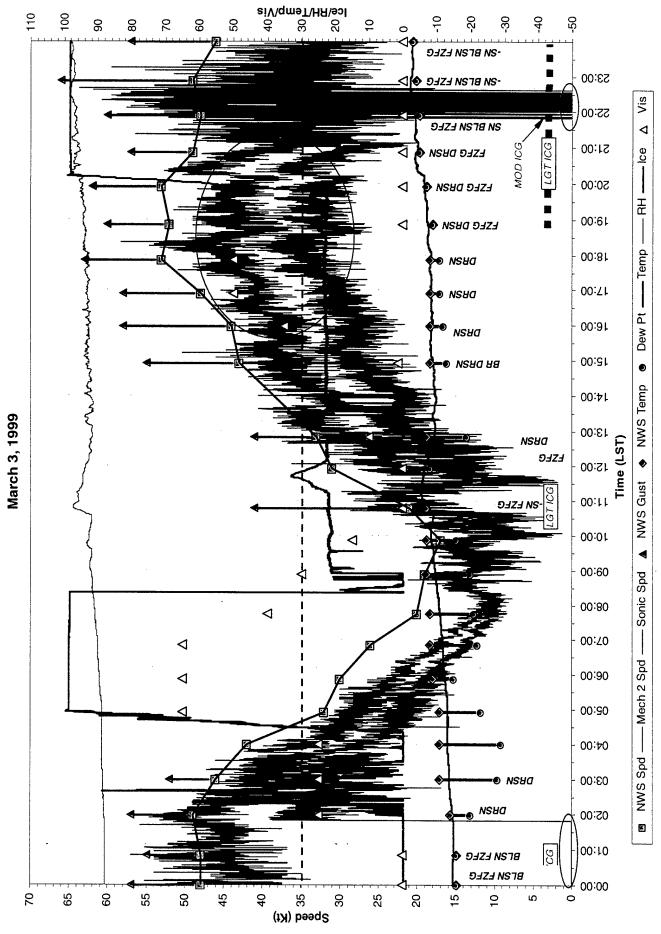
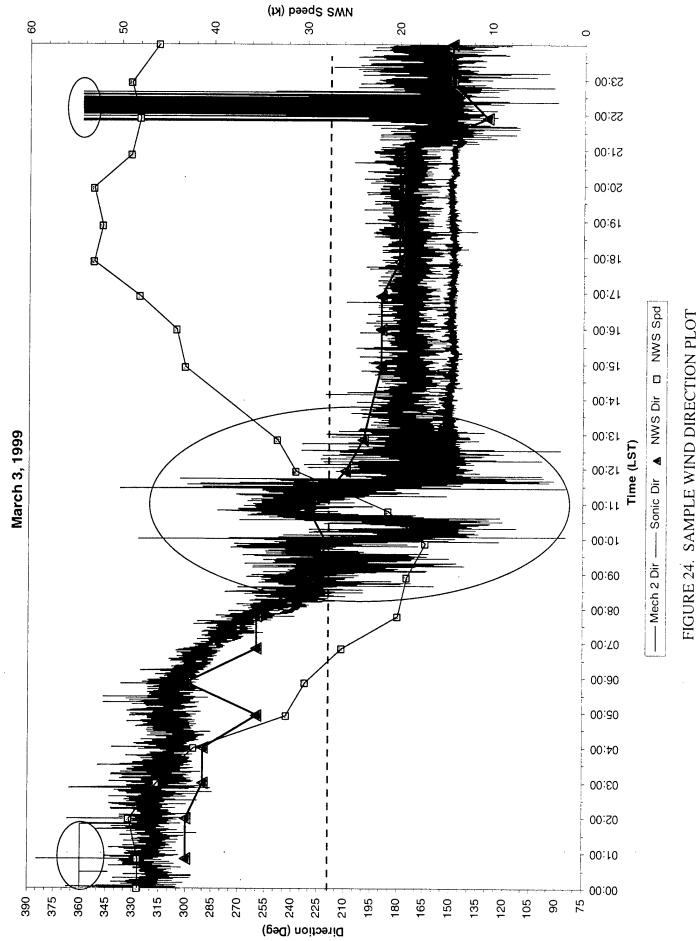


FIGURE 23. SAMPLE WIND SPEED PLOT



on the secondary ordinate axis. Drop lines depict the spread between the observed wind speed and gust values, and the observed temperature and dew point temperature. Text from the Present Weather field in the hourly surface observations is also indicated as the vertically aligned italicized text which is generally positioned below the temperature values. Additional icing information extracted from the Remarks field is indicated as light blue graphics and horizontally aligned italicized text at the bottom of the plots. Finally, ovals are added to point out particular cases and features of interest, which are discussed further in the text.

The second daily plot shows the direction vane, sonic, and observed wind directions along the primary ordinate axis. Sonic wind directions are plotted over the vane direction values. For reference, corresponding observed wind speed values are displayed according to the secondary ordinate axis. Red-dashed horizontal baselines are used to represent the azimuth orientation corresponding to the longitudinal axis of the test bed-mounting fixture. Ovals are used to point out particular cases and features further discussed in the text.

4.4 RESULTS/DISCUSSION.

A summary of the data collected over the 37-day study is presented appendix A. This overview breaks out the daily test bed data into separate cases according to prevailing weather conditions, and various wind, temperature, and relative humidity scenarios. The hourly mean and standard deviation values of the observed and computed weather parameters, along with corresponding hourly surface observations, are provided in appendix B. Excel worksheets showing the times series plots are given in the figures supplied in appendix C. Because of the large volume of data in these two appendices, they are provided as separate attachments to this report and are available through ACT-320. Output text files representing the time series of 10-s averaged observed and computed weather data are also available through ACT-320.

As previously mentioned, video images were not available for monitoring the test bed and wind sensors. This presented the largest shortcoming of the study, as there was no way to correlate sensor data and positively verify the existence and extent of icing on the sensors. Other difficulties encountered are noted in following paragraphs.

4.4.1 Ice Sensor.

Inspection of the plots shows that the behavior of the ice detector was erratic on occasions during the demonstration program. The time series are not consistent with the expected nominal response shown in figure 10. For instance, data for the period February 13–14, 1999, shows extended periods of observed icing, but the sensor output remained high without tripping the probes deicing heater. On other occasions, the sensor intermittently attempts to deice itself. Similar behavior is shown for the light icing period February 17–18, 1999. By the time the sensor's output voltage reaches 100 percent, the heater should be activated regardless of the external conditions. Further review of the data indicates there may have been a problem with the heater control system, as maximum output voltages of 6.8 volts direct current (Vdc) were recorded, which is greater than the sensor's 5 Vdc output voltage specification. Sensor performance may have also been affected by excessive ice buildup immediately around the probe caused by the flanges and rough edges associated with the I-beam and specially fabricated sensor

housing (see figure 9). The beam and unheated housing may have promoted the formation of ice around, rather than on, the probe. Original plans had called for wrapping the sensor housing with commercial heat tape; however, none was available through local vendors at the time of installation. For any future efforts, the housing should be wrapped with heat tape or the design modified to prevent excessive ice and snow build up. Alternate ice detection technologies should also be considered.

4.4.2 Relative Humidity Sensor.

The integrated air temperature and relative humidity probe also displayed erratic behavior on occasion during the demonstration program. A reasonable response for the relative humidity sensor, which is consistent with the observed dew point temperatures, is shown for February 27–28, 1999. However, erratic relative humidity response was noted on other occasions, particularly for February 25, 1999. The setup of the sensor was subsequently reviewed. The probe and radiation shield were mounted in a specially fabricated aluminum canister which was open at the bottom and approximately 0.5 m (1.5 feet) above the ground. Examination of figure 6 shows the test bed with snow and snowdrifts prior to installation of the sensors. The figure suggests that snow accumulation about the sensor housing may have closed off the bottom opening or contributed to ice buildup from below the canister. In any future effort, the canister should be raised in order to be unaffected by blowing and drifting snow.

4.4.3 Test bed Server.

Some problems with the remote access of the test bed server were experienced. Data collected and recorded during the period March 15–20, 1999, were sampled at different sample rates. Closer examination of the raw data for the 5-day period indicates that the datalogger and sonic sensor data sampling rates were erratic and consistently less than normal. During this period, the sonic sensor and datalogger sampling rates varied at about 1–5 and 7–13 s, respectively, whereas the corresponding nominal sampling rates are approximately fixed at 1 and 10 s. Based on a log of remote access activities, it was determined that the data acquisition process was affected, perhaps due to an errant process in the PC software following an unsuccessful remote login attempt.

4.4.4 Wind Sensors.

Sufficient data was collected during the effort to derive some useful results and preliminary conclusions on the wind sensor performance. Because of the expected and unexpected test bed limitations as well as the unavailability of the video camera, it is recognized that caution should be used in making any hard conclusions concerning the performance of the wind sensors. It is also noted that the sonic sensor was a prototype unit and no performance levels were implied or guaranteed by the manufacturer.

4.4.4.1 Mechanical Sensors.

During the course of installation and testing, several problems were encountered with the Number 1 rotor anemometer and direction vane. First, during installation, the rotor heater controller failed. Because the rotor anemometer was considered the more important of the two for testing, the direction vane heater controller was used to operate the rotor anemometer heater.

This rendered the direction vane heater inoperable, and consequently, the Number 1 direction vane was considered out of service. The Number 1 anemometer was operational at the completion of the installation. However, a total mechanical failure of the Number 1 rotor anemometer was subsequently experienced early in the study. It was found that the failure was due to excessive heater output resulting in damage to the rotor bearing assembly. The sensor and controller were subsequently removed and returned to the manufacturer.

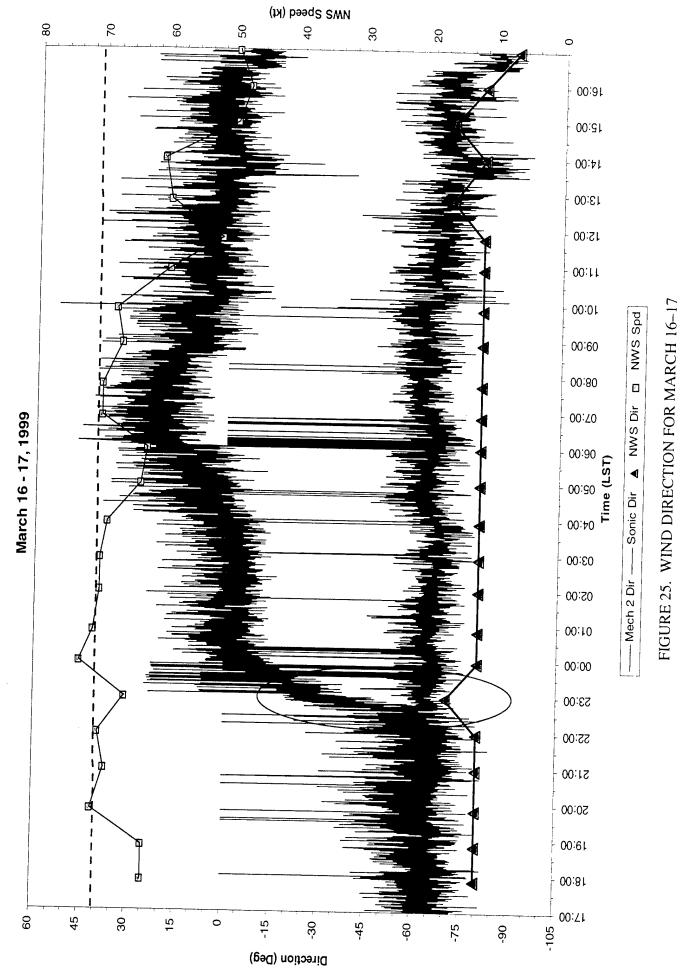
Collected data indicates that on March 16, 1999, the mounting adapter of the Number 2 direction vane apparently loosened and turned during conditions in which the sensor had been experiencing sustained 60 kn winds and gusts to 90 kn, over the 14-hour period leading up to the event. The onset of this event is shown in figure 25. The result was an ~70° error in position throughout the remainder of the study, as indicated in the plots.

The plots were analyzed in light of the effects of the wind sensors on one another when winds were parallel to the longitudinal axis of the test bed-mounting fixture (see figure 3). Effects of the ultrasonic and the Number 2 mechanical sensors as the most leeward sensors of the array are illustrated in figures 23 and 24. These figures show the March 3, 1999, wind speeds and directions when the wind became approximately 220° and parallel to the test bed beginning at about 0900 Local Standard Time (LST). A pronounced effect was noted for the leeward sensors. This effect was anticipated because of the likelihood that significant ice masses would grow on the failed and inactive Number 1 sensors and masts. The plots in appendix C show this effect was also experienced on February 18, and on March 1, 4, and 6, 1999. On the other hand, little effect is seen when the winds are about 40° and the Mechanical 2 and ultrasonic sensors are effectively the windward sensors of the array, as experienced on March 10–11, 1999.

In general, good agreement among the wind sensors was seen for fair weather conditions, although a bias in wind direction differences among the wind sensors was observed. A small bias could be expected due to the sensor installation and the estimation procedure used to achieve azimuth alignment of the sensors; however, there are extended periods when the rotor wind speeds are consistently greater than the sonic wind speeds by as much as 10 kn or more. The possibility exists that ice forming on unheated or insufficiently heated surfaces could have disturbed airflow around one or both sensors.

Results for light winds are shown for February 19–21, 24–25, and March 11–14, 1999. In general, there is more wind direction variability for the mechanical direction vane than for the sonic sensor, especially for wind speeds greater than about 35 km as shown for February 26, 1999.

An unusual event was noted for the direction vane during the period 0030–1100 LST on March 5, 1999. A time series of the wind direction data and the corresponding wind direction frequency histogram for the period are shown in figure 26. The figure shows a skewed wind direction distribution for the mechanical sensor indicating that the azimuthal movement of the direction vane was limited at ~318°. This effect may indicate the presence of an interfering ice formation on the southeast side of the sensor head stemming up and around from the sensor's mast. This observation is consistent with data shown for March 4, 1999, which shows that winds were consistently from ~150° under snow, freezing rain, and light icing conditions for a 12-hour period before the wind began to move back around to the north. It should be noted that the sonic



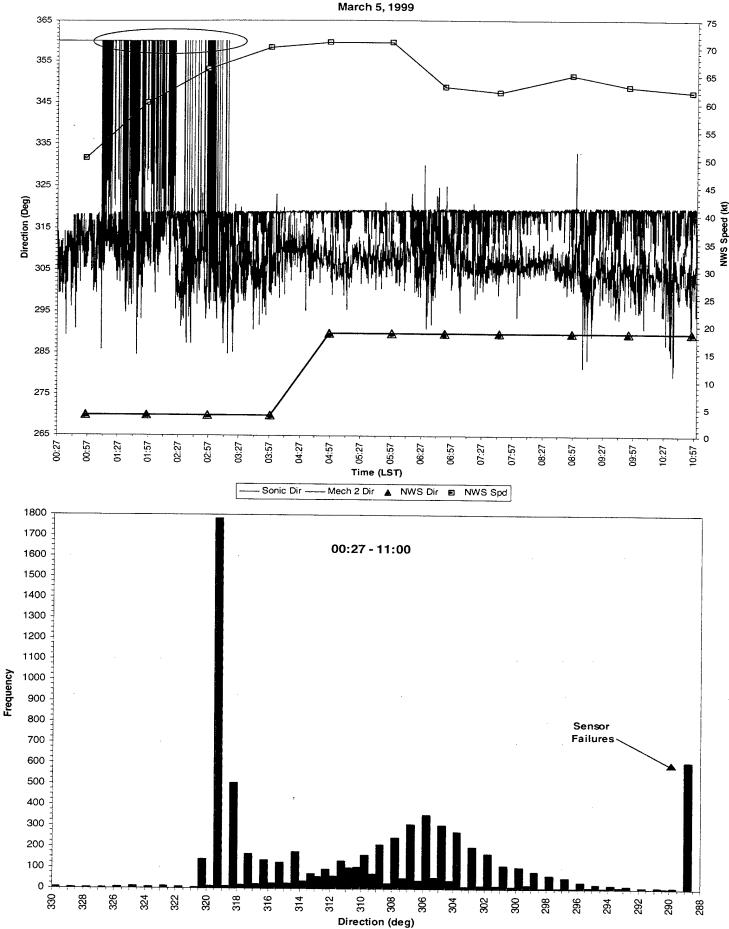


FIGURE 26. WIND DIRECTION DISTRIBUTION FOR 0027–1100 LST ON MARCH 5

sensor experienced a significant number of failures (~16 percent) during this period. Rime icing of the sensors was highly probable during this period, and is the likely cause of the failures.

Anomalies in the rotor speed were also noted for the approximately 13-hour period from 2000 LST on March 15, through 0845 on March 16, 1999, during which the present weather indicated snow, blowing snow, freezing fog, and light icing. Wind speeds for the period are shown in figure 27. During this period the mechanical sensor wind speeds dropped off to about 10–20 kn while observations indicated winds from 50–80 kn winds, gusting to almost 120 kn. As indicated in the figure, the sonic sensor experienced a significant number of failures also during this period. Again, conditions for rime icing were favorable and are the likely cause of the failures. It is not clear whether the slowing of the rotor anemometer was caused by ice accumulating on the rotor itself, or building up from the unheated mast below.

4.4.4.2 Ultrasonic Sensor.

Results of the ultrasonic sensor were reviewed. From the 37 days of data retrieved, a total of 742 hours (~31 days) of sonic anemometer data were recorded and collected. This sensor experienced a significant amount of data failures (total ~66 hours) throughout the experiment and was effectively unavailable approximately 9 percent of the time. A failure qualifies as a bad data flag received from the sensor as a result of unreliable readings. The failures appear highly correlated to snow and icing conditions. Collected data indicates the sensor experiences a large number of failures when there is light to moderate snow (including drifting and blowing snow), and icing, under certain wind and temperature conditions. The failures during these events are generally intermittent in nature, with frequencies proportional to the severity of the weather conditions. However, inspection of the plots shows there were instances where the sensor was in complete failure-mode over periods ranging from 2 to 3 continuous hours.

There were a significant number of these snow and icing events where the sensor was wandering in and out of failure mode (see February 28, and March 2, 4, 7, 8, 15–16, 1999). It should also be noted here that there were a number of occasions where the sensor was intermittently reporting supposedly valid data, and the data was found to be inaccurate and unreliable. An extreme case of this was found for March 7, 1999. On this occasion, the sensor was primarily in failure mode from about 1845–1930 LST because of a typical blowing-snow and light-icing event. During this period there were a few 'valid' sonic reports (sensor flag as Pass) which appear to be somewhat reasonable. However, there were also a number of 'valid' wind speed reports that ranged from 246 to 345 mph. In total, there were approximately 11.5 minutes of 1-second samples of sonic data where the data was greater than the sensor's reported operational range of 144 mph. Although this was the only extreme scenario found in the entire dataset, additional unreasonable data values were found on March 16, 19–20, 1999.

At this time, the exact cause of the sensor failures and inaccurate data are not known. Causes may be either rime ice buildup on or near the sensor transducers or the effects of precipitation and freezing fog traveling through the sensor sampling volume. Observed errors could also be caused by shadow effects of ice growing up from the sensor mast, or flow distortion around the sensor assembly from nearby sensors. It may also be possible that the heater output and/or duration may not be powerful enough to melt the ice, since the most significant number of

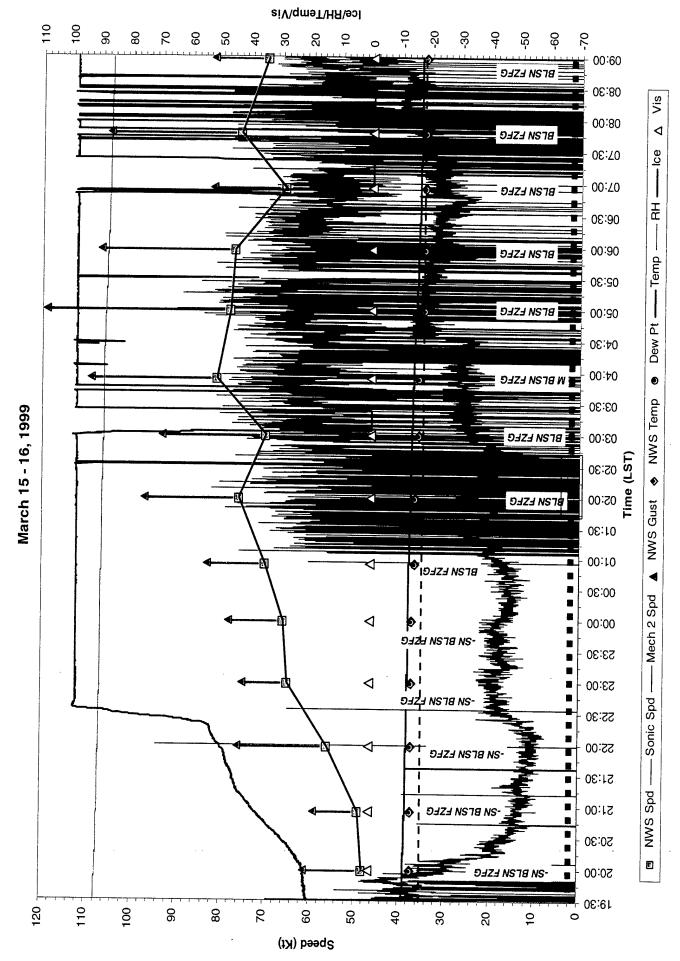


FIGURE 27. WIND SPEED FOR MARCH 15-16

failures occurred during icing events. Unfortunately, the difficulties encountered with the installation and operation of the video camera prevented the determination of which of the above scenarios, if any, is correct.

5. CONCLUSIONS.

This test effort was considered a preliminary survey and shakedown exercise, as a number of test assumptions including scheduling and setup limitations were understood before installation of the test bed. Funding delays resulted in slips in planning, coordination, and schedule. The installation was delayed until February, and took place during unfavorable weather conditions. The first 3 months of the winter season were consequently missed, and a burn-in period, which might have identified some of the problems with the test suite, was not available.

5.1 TEST BED SETUP.

The test site is remote, and it is recognized that the test methodology and setup for a similar and future effort could be improved and better controlled. Several needed enhancements to the test bed setup were identified, including the need for calibration and alignment procedures, better sensor siting, and improved equipment enclosure designs for the ice detector and the temperature and relative humidity sensors. Although the local and remote data collection and communications design and setup proved to be reliable, the need for a few improvements to the remote access of the test bed server and communications were also noted. Overall, a number of test setup, control, and data collection issues were identified and noted for preparation of a proposed follow-up effort.

5.2 WIND SENSOR PERFORMANCE.

Inspection of the data shows that the wind sensors were affected under certain snow and icing conditions. The sonic sensor experienced a significant amount of data failures throughout the experiment, and was effectively unavailable approximately 9 percent of the time. The failures are highly correlated to snow and icing conditions. In addition to the intermittent and long duration failures, there were instances when the sensor reported unrealistic wind speed values beyond the operational range of the sensor—but were declared as valid by the sensor. The sensor's internal quality control firmware should be flagging this obviously erroneous data. It is clear from the data that modification and further testing of the ultrasonic sensor would be needed before consideration for use in the Wind Hazard Information System (WHIS). Data and results in this report also suggest that, although the mechanical sensors may be suitably heated, large ice formations may grow up from the unheated sensor masts and consequently shield and affect the performance of these sensors.

6. RECOMMENDATIONS.

Based on the findings of the demonstration program, it is recommended that a larger scale and more controlled evaluation of several types of wind sensor technologies and sensors be performed on Mt. Washington in the winter of 2000–2001. The test bed would be set up in similar fashion as was done for the 1999 demonstration program, except the specific

improvements noted in this report would be incorporated to ensure a more controlled assessment. This would include improved sensor housing and siting considerations, investigation of an alternative ice detection sensor, and a more reliable video camera. Since it is realized that the success of this proposed study would require a reliable and robust instrument, alternative means for mounting the video camera would be assessed. Other cameras would also be considered. Finally, efforts would be made to secure cleaner electrical power and signal communications to the heated shelter, and test bed instruments and equipment. Additional planning considerations would include commercial grade or National Electrical Manufacturers Association (NEMA)-rated environmental instrument enclosures. The on-line monitoring, and data reduction and analysis tools, including the software and plotting programs developed for the 1999 demonstration would be used to monitor, analyze, and present the data.

It is recommended that the ultrasonic heated anemometer be reevaluated. It is expected that, if the conditions surrounding data failures could be clearly defined and linked to the sensor itself, the manufacturer might be willing to consider signal processing and heater modifications to correct the failures and marginal sensor performance noted during the demonstration. This would allow for consideration of alternate sensors for use in the Wind Hazard Information System (WHIS). The mechanical sensors should also be reevaluated to verify the performance and reliability of the rotor anemometer, which failed during the demonstration program. A more positive means of mounting the direction vanes should be investigated as it was found that the sensor-mounting adapter set screws came loose from the pipe stub mast during the experiment.

In addition, it is recommended that the scope of the study be extended to verify the performance of other wind sensor modifications, models, and technologies. Based on another recent study and wind tunnel tests, the manufacturer of the mechanical wind sensor is considering a modified sensor with longer rotor ears. The purpose of this modification is to enhance the response and performance of the sensor when there is a vertical component of wind. Because of the heater requirements and new larger-ear design, it is suggested that this new sensor also be installed and evaluated to study effects of snow and icing conditions. The manufacturer of the mechanical sensors is also considering the development of a new propeller-vane type design. If a prototype is produced, it should also be procured and evaluated during the proposed study. Current discussions also suggest there is a new laser wind sensor device that Michigan Aerospace Corporation has designed for the Air Force. Since this device may have potential application to ground-based weather observing systems such as the Juneau WHIS, procurement and test of this sensor should be considered.

Because wind sensor mounting fixtures and masts can influence the buildup of ice on and around the sensors, it is recommended that modifications to the design of the masts be investigated. Currently the Juneau wind system installation uses commercial heat tape to keep the wind sensor masts ice-free. It is suggested that the reliability and feasibility of this, and alternative technologies to keep sensors ice-free, be explored in the proposed study. Finally, in light of the fact that vertical wind components are likely to be present in the mountainous terrain where the Juneau WHIS sensors are mounted, it is suggested that the proposed effort also attempt to quantify sensor response to off-axis winds.

7. ACRONYMS AND ABBREVIATIONS.

AMS Acquisition Management System

AWR Aviation Weather Research

FAA Federal Aviation Administration

ft foot

FTP File Transfer Protocol

in inch

IP Internet Protocol

kHz kilohertz

kn knot

LST Local Standard Time

m meter

m·s⁻¹ meters per second

METAR Aviation Routine Weather Report

mm millimeter

mph mile per hour

MWO Mt. Washington Observatory

NCAR National Center for Atmospheric Research

NEMA National Electrical Manufacturers Association

OT Operational Test

PC personal computer

PDT Product Development Team

s second

Vdc volts direct current

W watt

WHIS Wind Hazard Information System

APPENDIX A DATA LOG AND SUMMARY

APPENDIX A

DATA LOG AND SUMMARY

			Wi	nd	Temp	RH	
Date	Case	Weather	Direction (deg)	Speed (kt)	(°C)	(%)	
	1	FZRA, FZFG, ICG	260	40	0	98	
2/12	2		220	35	7	77	
	3	FZRA, FZFG, ICG	235	15	3	98	
	4	-SN, FZFG, ICG	270	20	-10	93	
2/13	5	FZFG, ICG	260	35	-14	89	
2/10	6	-SHSN, FZFG, ICG	270	30	-15	87	
	7	-SN, FZFG, ICG	300	09	-20	84	
2/14	8	0,1,1210,100	340	20	-18	85	
2/16	9		270	21	-6	80	
	10		260	16	-6	70	
2/17	11	-SN, FZFG, ICG	180	32	-8	94	
	12	FZFG, ICG	200	22	-7	94	
2/18	13	-SN, FZFG, ICG	260	25	-5	95	
	14	FZFG, ICG	300	19	-11	91	
2/19	15	1. 2. 0, 100	300	08	-11	91	
2/10	16		130	03	-11	89	
2/20	17		020	05	-8	77	
_,	18	FZFG, ICG	360	06	-15	89	
	19	-SN, FZFG	340	20	-16	89	
2/21	20	011,1210	340	12	-17	50	
_,	21	FZFG, ICG	310	09	-20	82	
	22	1 2 3, 10 3	320	15	-23	30	
2/22	23	DRSN	320	38	-24	47	
	24		320	44	-23	33	
2/23	25		. 340	13	-18	45	
	26		060	07	-17	63	
2/24	27		090	23	-15	45	
	28		100	22	-15	50	
2/25	29	-SN, -SHSN, ICG	060	12	-12	80	
	30	-SN, BLSN, ICG	020	40	-11	90	
0/00	31	-SN, BLSN, FZFG, ICG	340	45	-13	89	
2/26	32	FZFG, ICG	310	63	-14	88	
0/07	33		310	53	-14	87	
2/27	34		310	12	-8	50	
0/00	35		170	35	-7	92	
2/28	36	-SN, BLSN, FZFG, ICG	150	50	-9	92	
0/4	37	FZRA, FZFG, GICG	150	42	-4	97	
3/1	38	-SN, FZRA, FZFG, GICG	180	12	-7	94	
0/2	39	-SN, FZFG, ICG	240	22	-10	91	
3/2	40	-SN, BLSN, FZFG, ICG	270	46	-14	90	
	41	BLSN, FZFG, ICG	290	47	-14	88	
3/3	42		260	20	-9	93	
-	43	DRSN, BLSN, FZFG, ICG	180	48	-8	97	

	4.4	F7D4 F7F0 0100	150	60	-1	99
	44	FZRA, FZFG, GICG		37	-9	95
3/4	45	SN, FZFG, ICG	170	18	- 1 1	93
	46	FZFG, ICG	230			90
	47	-SN, FZFG, ICG	270	35	-15	
	48	-SN, FZFG, ICG	270	65	-20	83
3/5	49	FZFG, ICG	290	65	-20	84
	50		290	35	-20	82
	51		275	30	-20	83
3/6	52	-SN, FZFG, ICG	230	19	-14	89
	53	-SN, FZFG, ICG	150	30	-15	88
3/7	54	-SN, FZFG, ICG	050	30	-17	87
3//	55	DRSN, BLSN, FZFG, ICG	310	50	-25	82
2/0	56	DRSN	320	67	-25	79
3/8	57		320	68	-22	82
2 /2	58		320	60	-20	83
3/9	59		340	12	-15	85
	60		330	13	-15	87
3/10	61	FZFG, ICG	010	22	-10	92
3/11	62	FZFG, -SN, DRSN, FZDZ, ICG	010	22	-7	94
3/11	63	FZFG, ICG	020	38	-7	95
3/12	64	FZFG, -SN, FZDZ, ICG	020	42	-6	96
0/12	65	FZFG, -SN , ICG	050	30	-8	95
	66	-SN, FZFG, ICG	050	15	-8	94
3/13	67	FZFG, ICG	340	20	-8	95
	68	FZFG, ICG	360	08	-10	93
3/14	69	FZFG, ICG	190	05	-10	99
3/17	70	-SN, FZFG, ICG	150	08	-10	97
	71	-SN, FZFG, ICG	110	08	-11	92
3/15	72	-SN, FZFG, ICG	330	50	-12	93
	73	BLSN, FZFG, ICG	320	75	-15	88
3/16	74	DRSN, FZFG, ICG	280	72	-12	91
	75	DRSN, FZFG, ICG	280	67	-9	93
3/17	76	DRSN, F2FG, ICG	270	50	-5	95
	77		260	40	-2	97
2/40		CN F7FC ICC	260	40	0	99
3/18	78	-SN, FZFG, ICG	270	60	-9	95
	79	-SN, BLSN, FZFG, ICG		56	-13	93
2/40	80	-SN, BLSN, FZFG, ICG	280 290	57	-13	91
3/19	81	BLSN, FZFG, ICG	300	46	-13	91
	82	-SN, BLSN		40		89
0,00	83	-SN, BLSN, FZFG, ICG	290	37	-14 -13	88
3/20	84	FZFG, ICG	290			90
	85		310	08	-12	
3/21	86	ON PROMETER 100	220	12	-14	89
	87	-SN, DRSN, BLSN, FZFG, ICG	170	50	-10	93

APPENDIX B TABLES OF RESULTS AND HOURLY SUMMARIES

ATE = 0212

INTMI	66	8	8	8	86
LGT THT O FG	01	Н	73	7	м
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ICG IK FZRAB35 LGT GICG PCPN VRY AERAB10 O HZ DSNT ALQDS NV VRY LGT RMK SHRAE1255 I DSNT ALQDS NOTY ALQDS I DSNT ALQDS NOTY LGT RMK TRS LWR SCT040 E-S F G EKNOOO FG INTMT V VIS 1/16V1/2 FG EKNOO MK PRESFR RAB35 MK PRESFR RAB35 RAEFZRAB25 VRY LGT GICG FZRAESNB20 LGT ICG T ICG T ICG	0	0	0	0	0
ICG K FZRAB35 LGT GICG ERAB10 HZ DSNT ALQDS V VRY LGT WK SHRAE1255 DSNT ALQDS VODS WIT TPS LWR SCT040 VIS 1/16V1/2 FG SCT EQ RESERR RAB35 VAFFZRAB55 VRY LGT GF FZRAESNB20 LGT ICG FZRAESNB20 LGT ICG FZRAESNB20 LGT ICG FZRAESNB20 LGT ICG	0	0	0	0	0
FERAB35 LGT (PB10) DSWT ALQDS (Y LGT SHRAE1255) TT ALQDS TPS LWR SCT ST 1/1 1/1 1/1 1/1 1/1 1/1 1/1 1/1 1/1 1/	0	0	0	0	0
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OSM FZFG VV000 M02, OSM -FZFR FZFG VV00 00 00 00 00 00 00 00 00 00 00 00 0	268	265 15	263 15	264 22	264 24
0SM FZFG 0SM -RA F 0SM -RA F 0SM -RA F 1 -RA FG V 0SM -SHR 0N -SHRA C 30SM -SHRA C 30SM -SHRA C 30SM -SHRA C 30SM FEWO 35SM BKN1 35SM BKN1 35SM BKN1 35SM BKN1 35SM BKN1 1/2SM FG 1/4SM FG 1/4SM FG 1/4SM FG 1/4SM FG 1/4SM FG 1/4SM FG 1/5SM FG 0SM FG VV 150V250 0 150V2	24	23	22	23	23
KT 0SM FZH KT 0SM -FA KT 0SM -RA KT 0SM -RA COSM -RA FG COSM -RA FG COSM -RA FG COSM -SHRA COSM -SRM COSM -SRM COSM -SRM COSM -SRM COSM -FC COSM -SN COSM	276 14	272 11	271 19	272 14	271 21
26038G48 26041G47 26037G41 26037G41 26037G41 240337G4 240337G4 240337G 220336G4 22036G4 22036G4 22036G4 22036G4 22036G4 22036G4 22036G4 22036G4 22036G4 22037G	74 34	24	23	23	21 1
1204572 1205582 1206552 1207542 1208522 1210532 121150	0	0	0	0	0
23557 000485 01558 01558 01558 01558 01558 01155	00-01	01-02	02-03	03-04	04-05

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77	77	77	77	22	0	0	0	4.2	7 m	m 73	r 7	2 3	0	0	0
12	11	13	9	118	0	0	0	11	9	8	36	34	0	0	0
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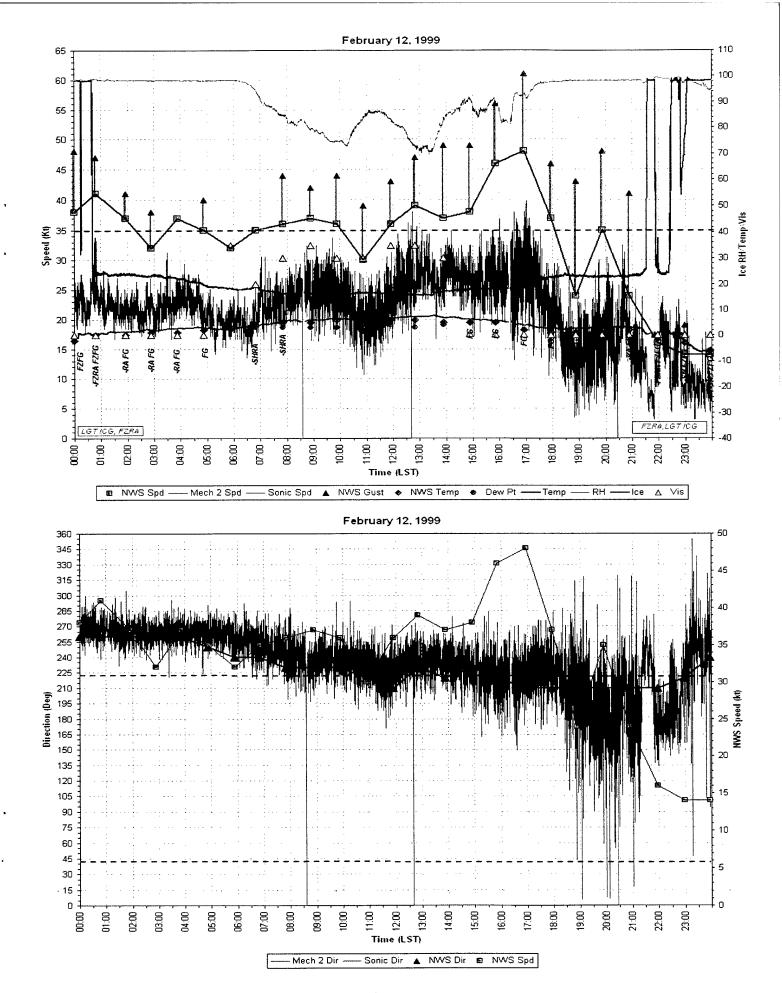
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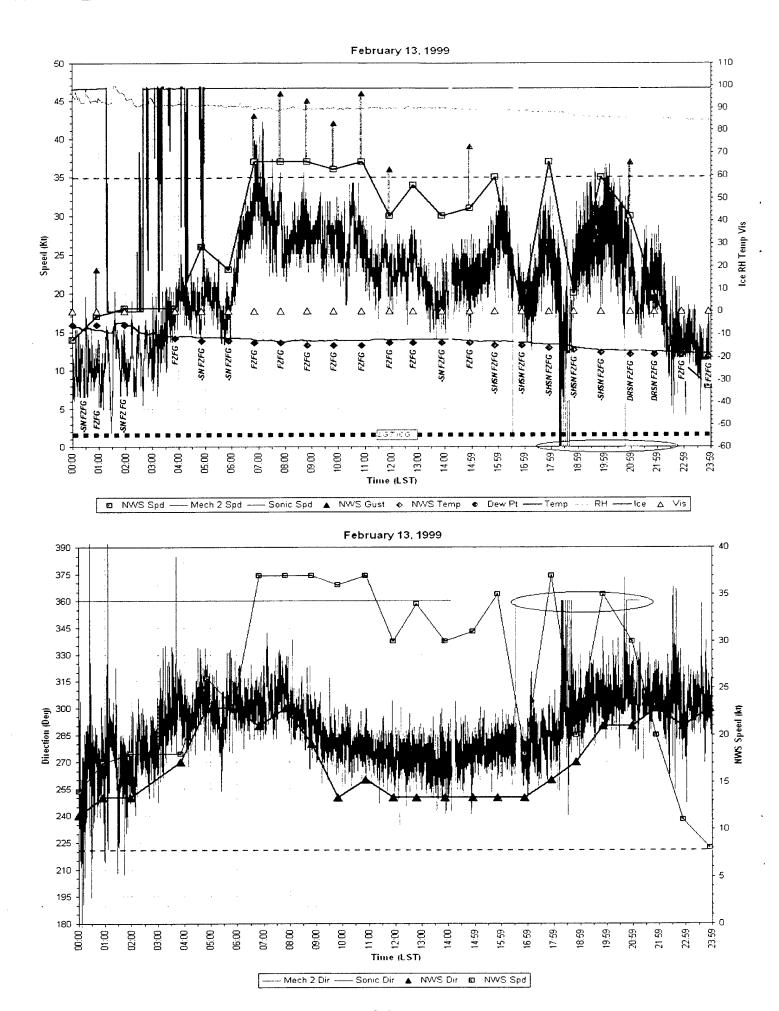
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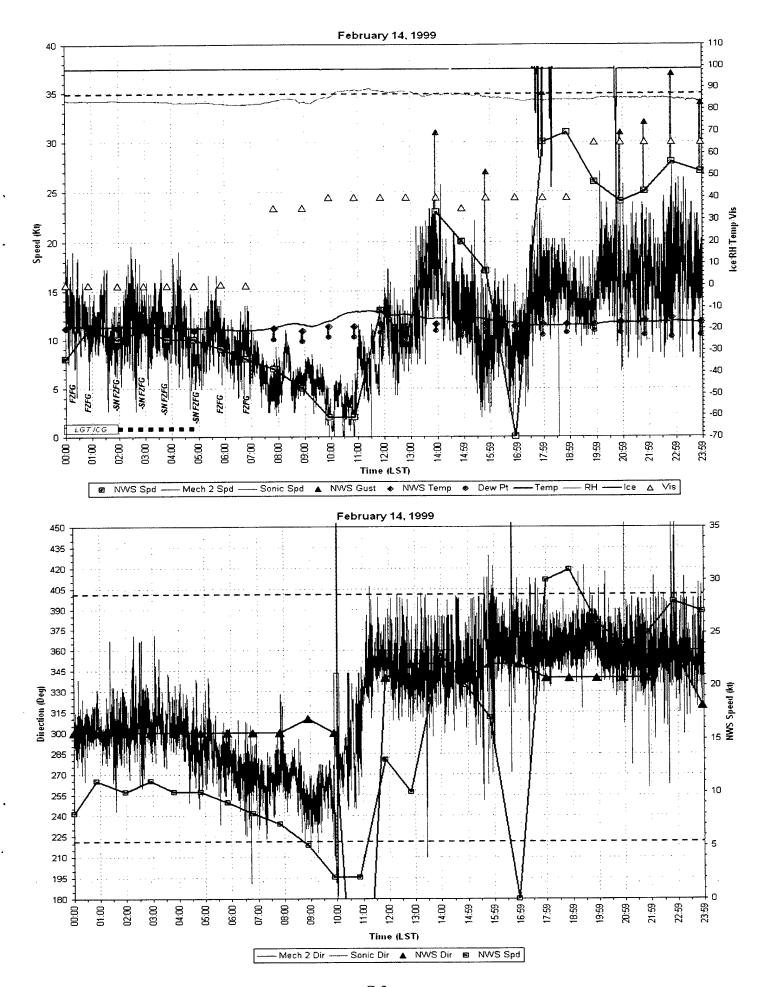
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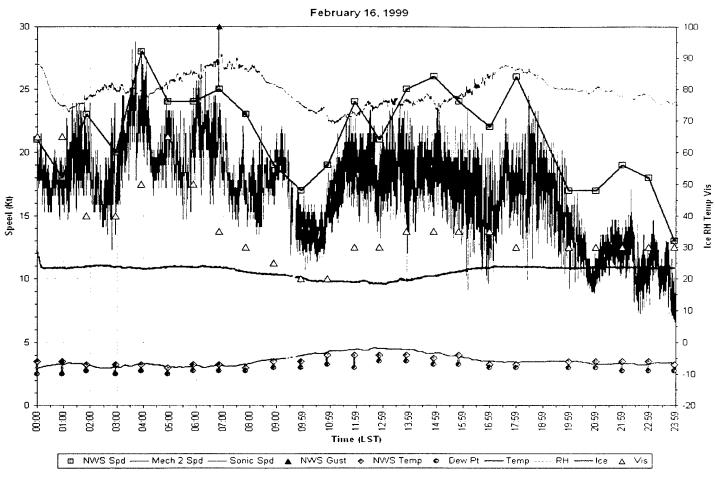
APPENDIX C

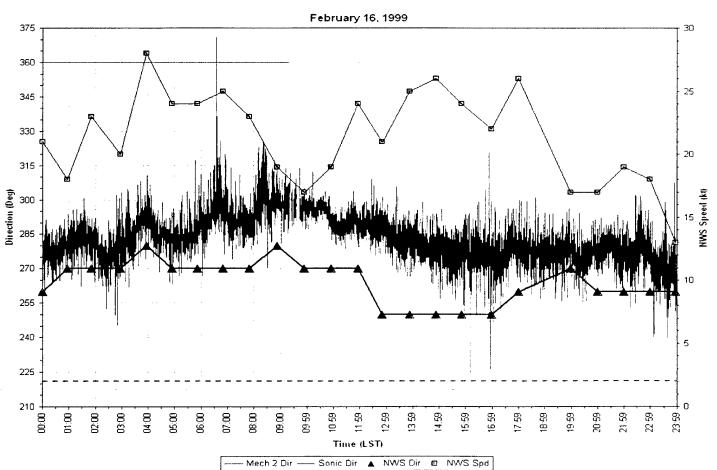
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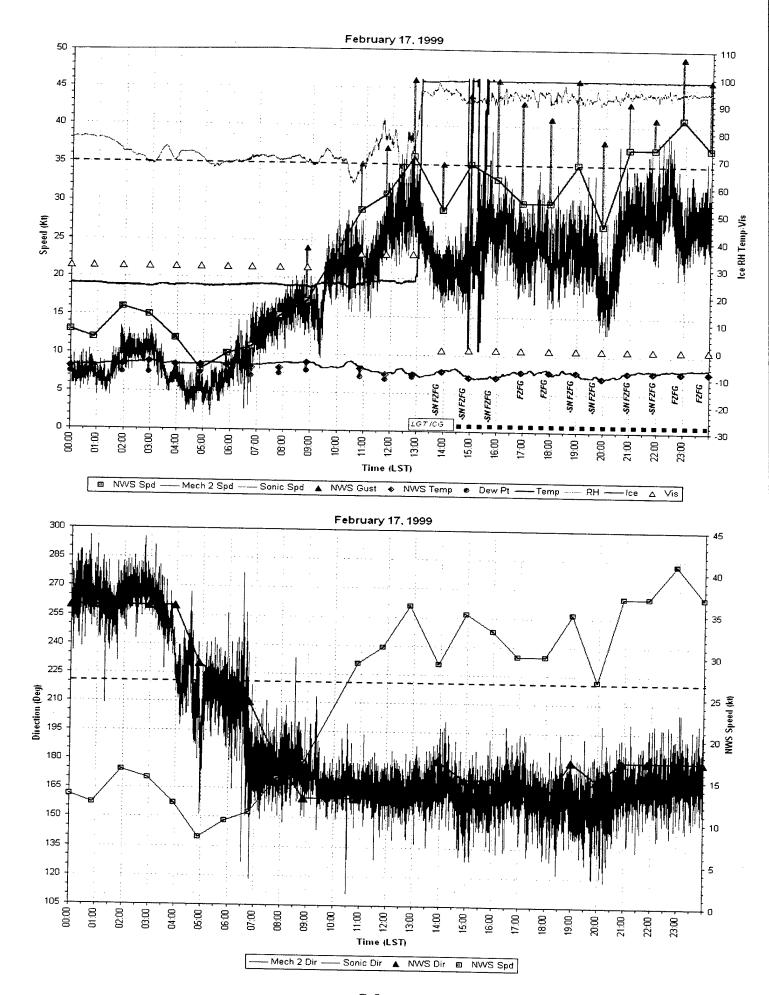


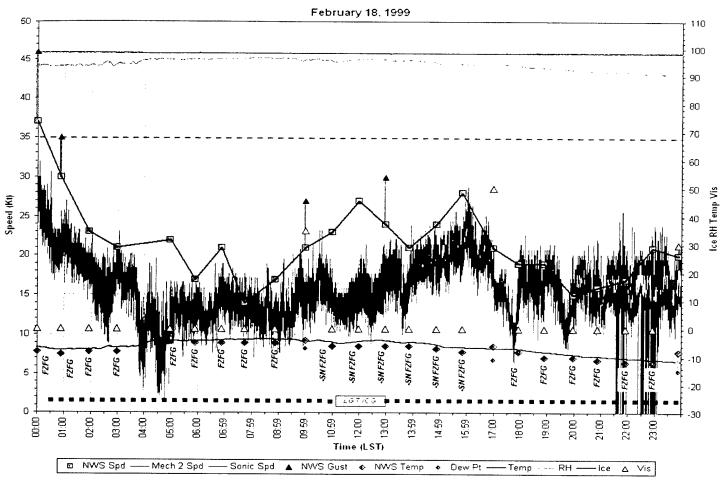


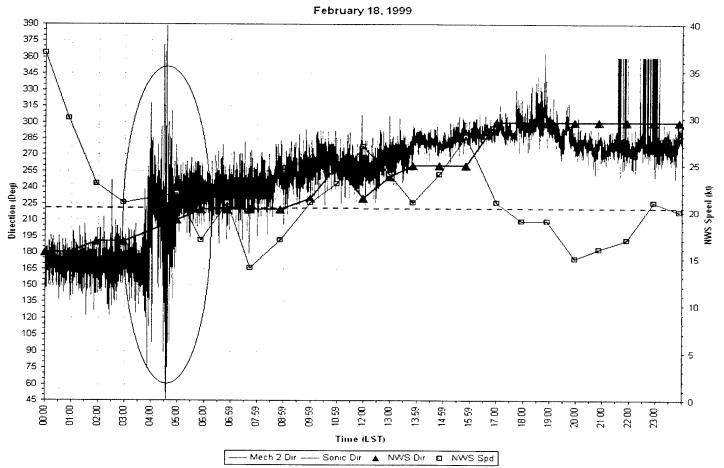


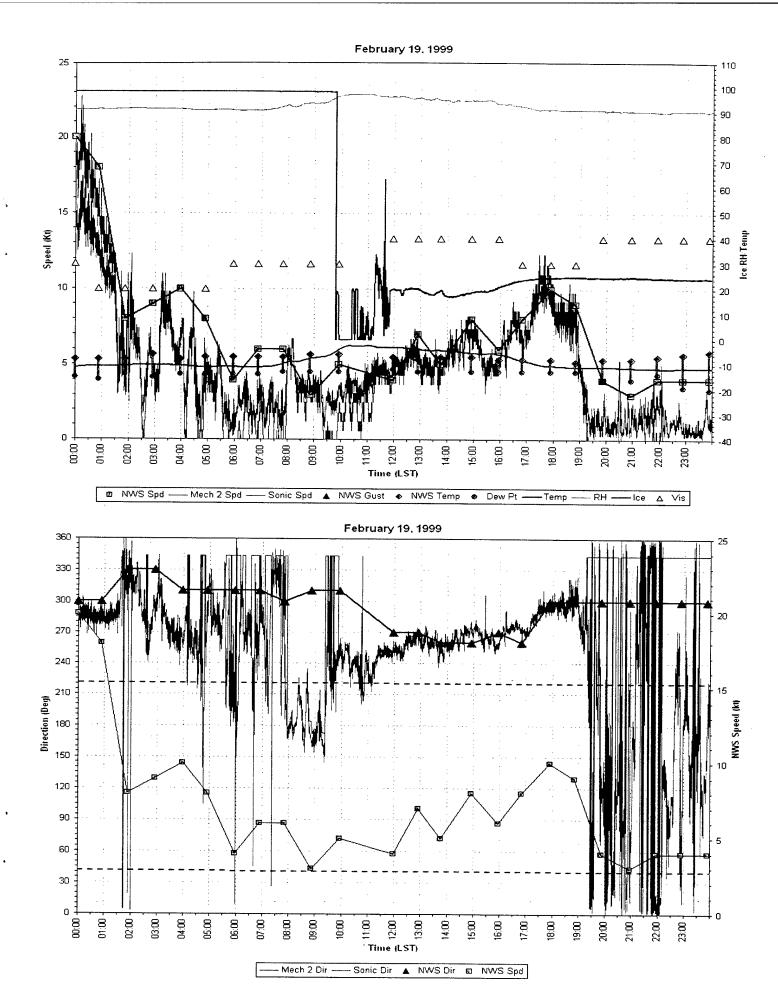


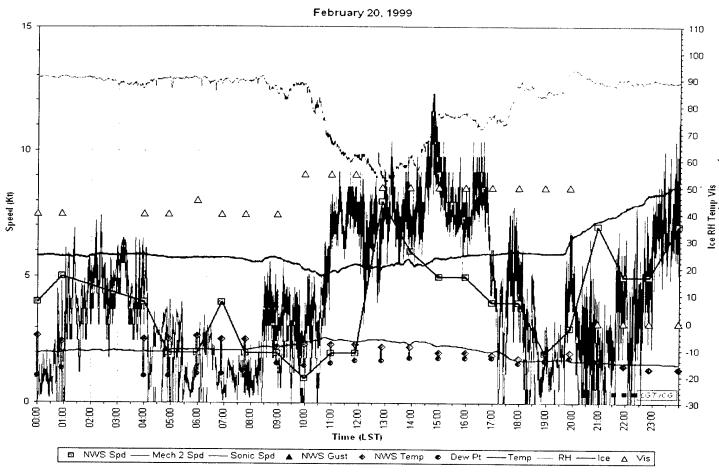


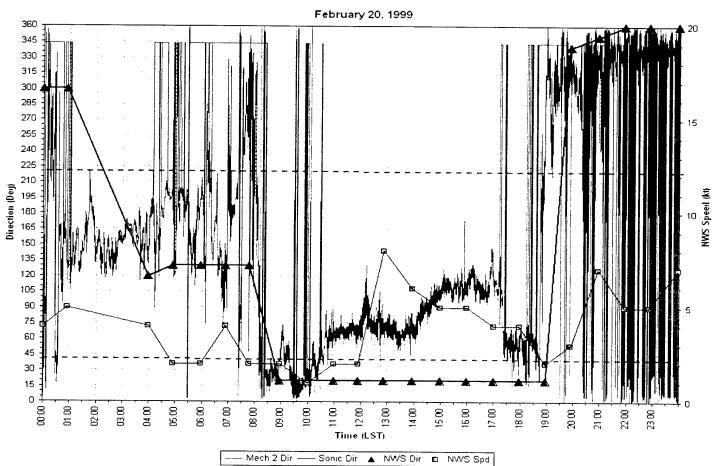


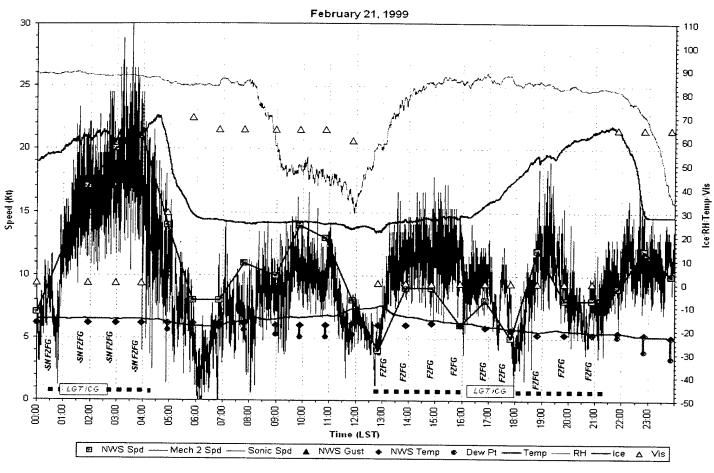


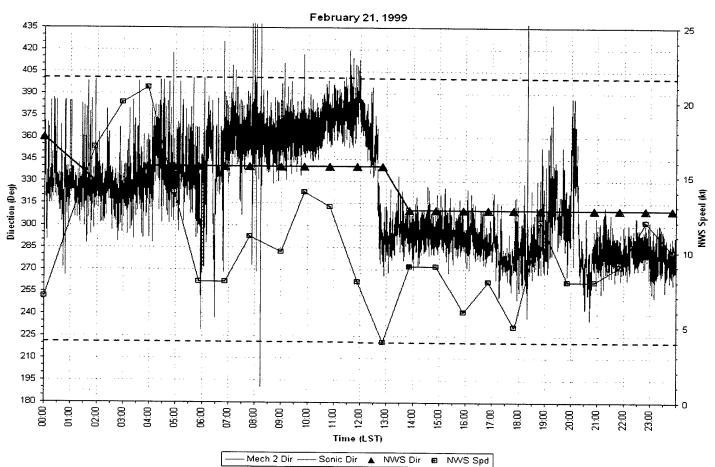


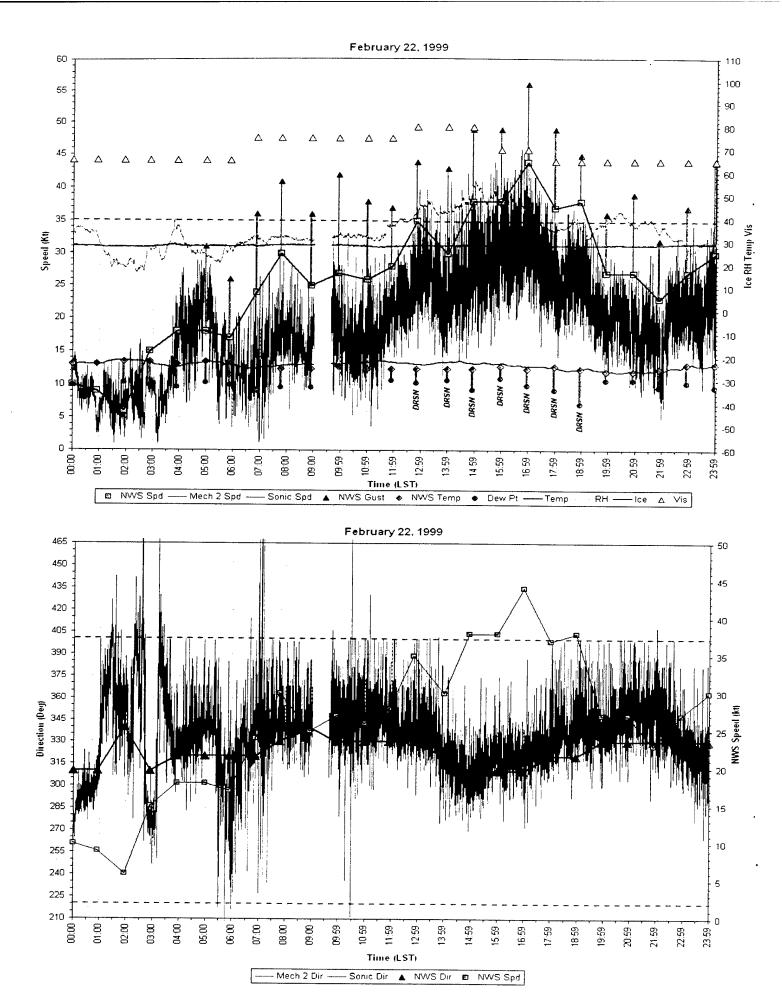


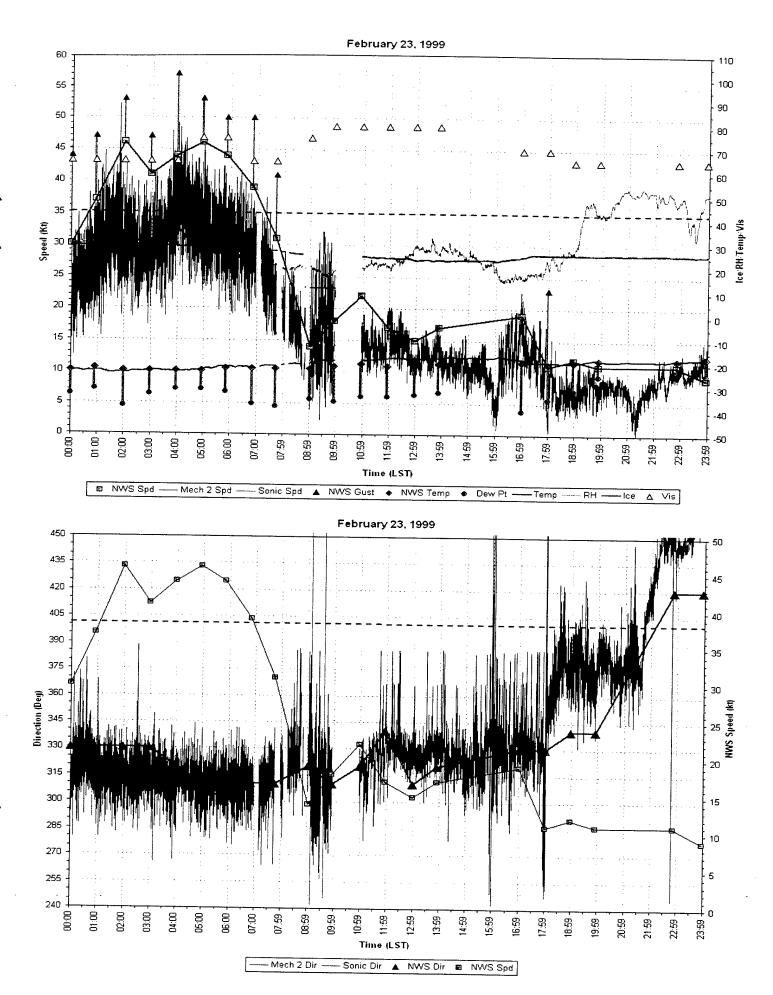


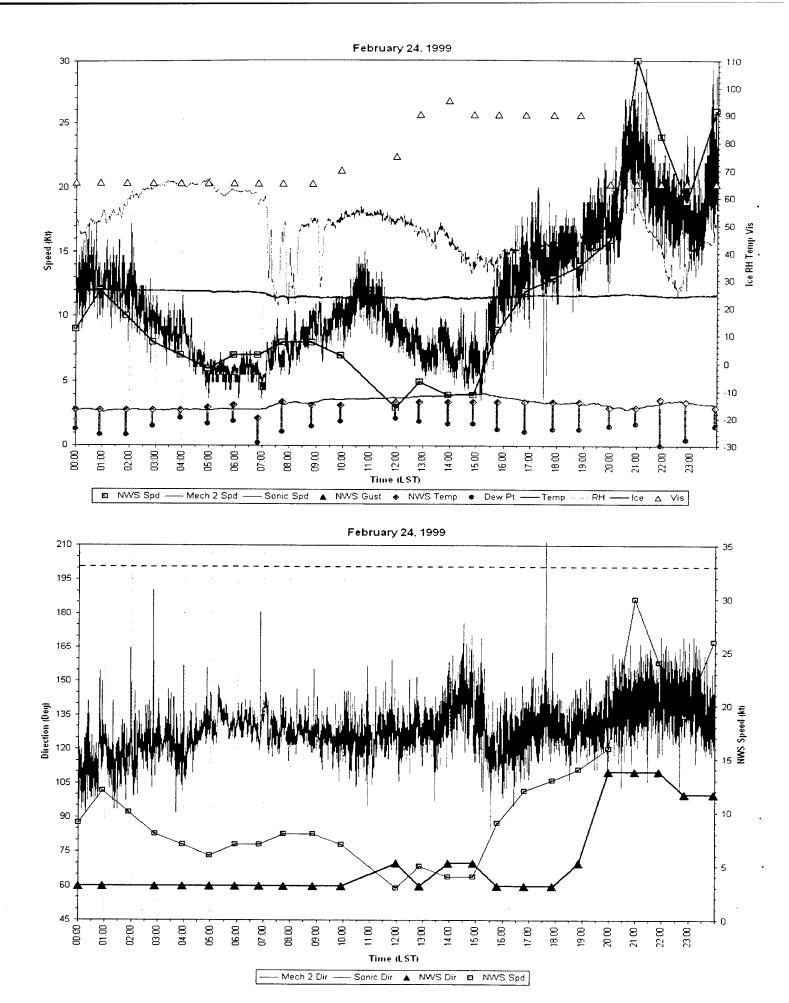


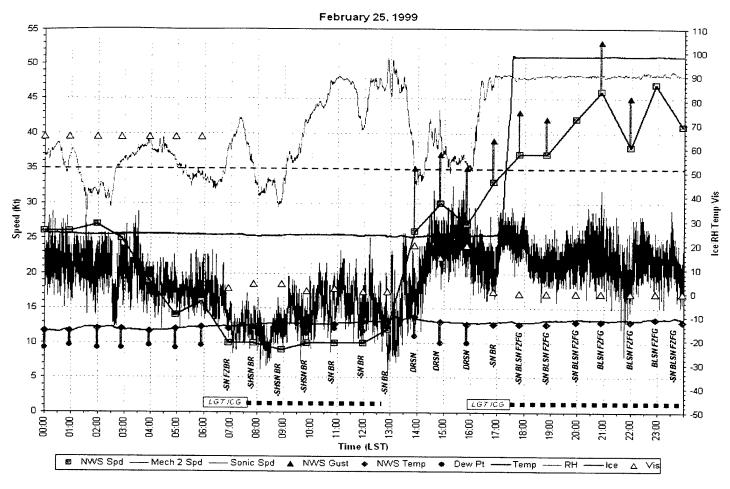


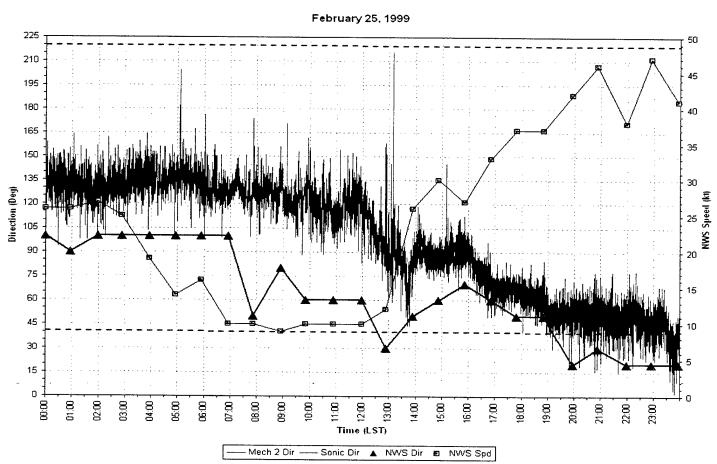


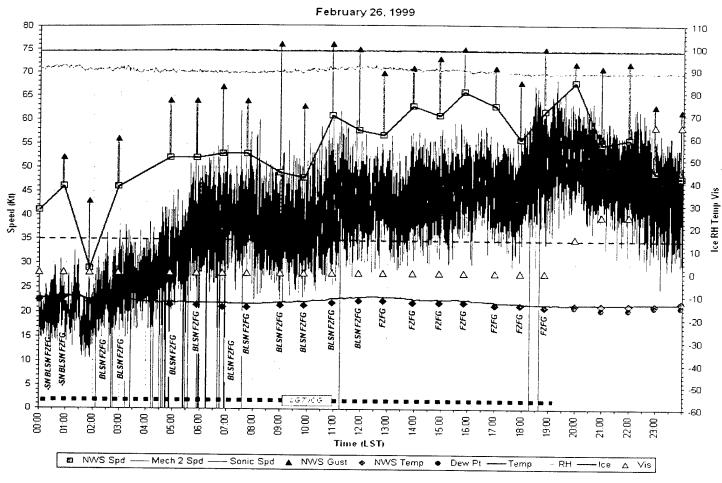


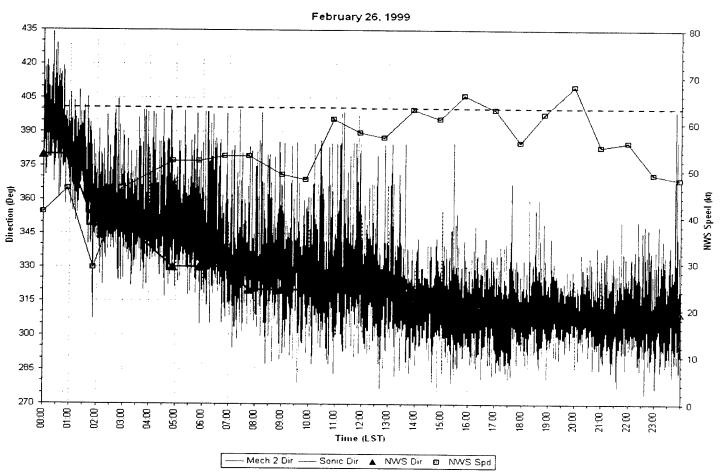


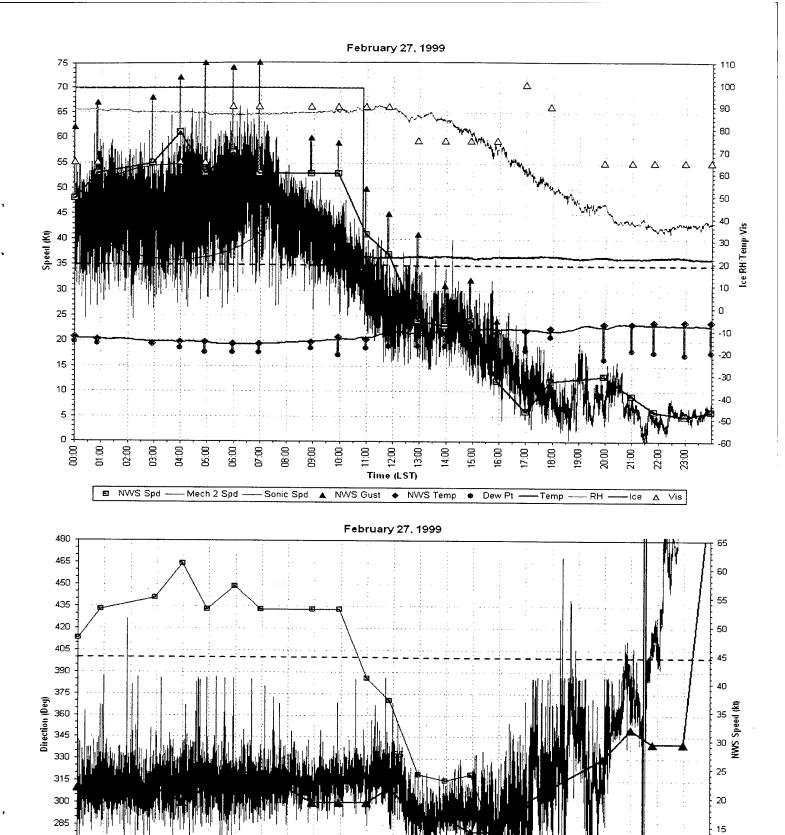












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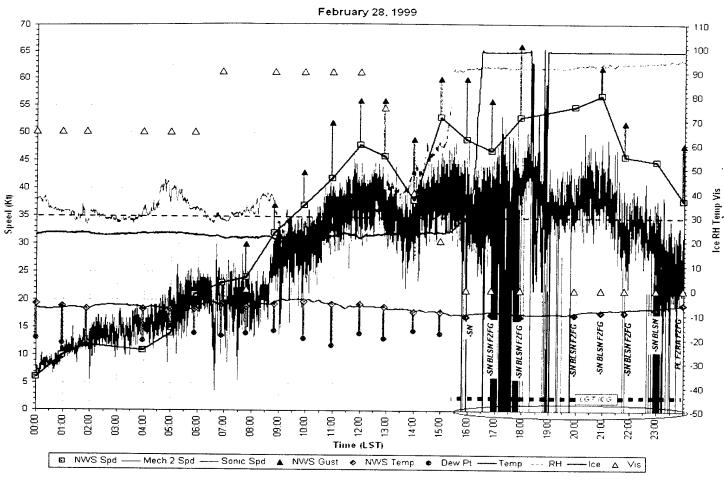
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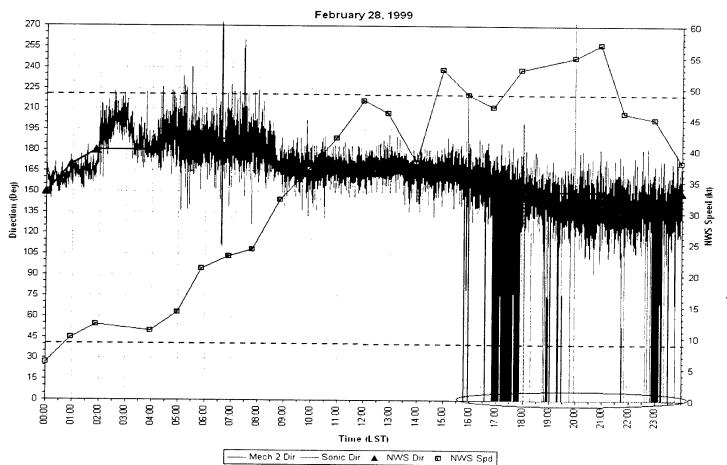
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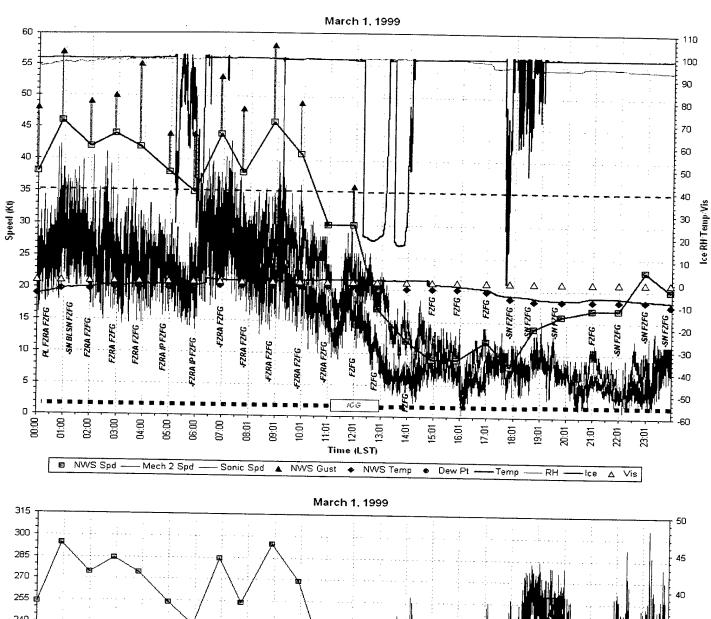
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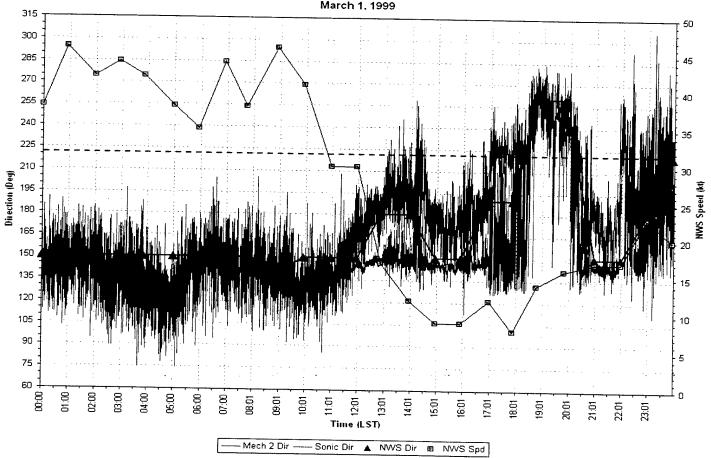
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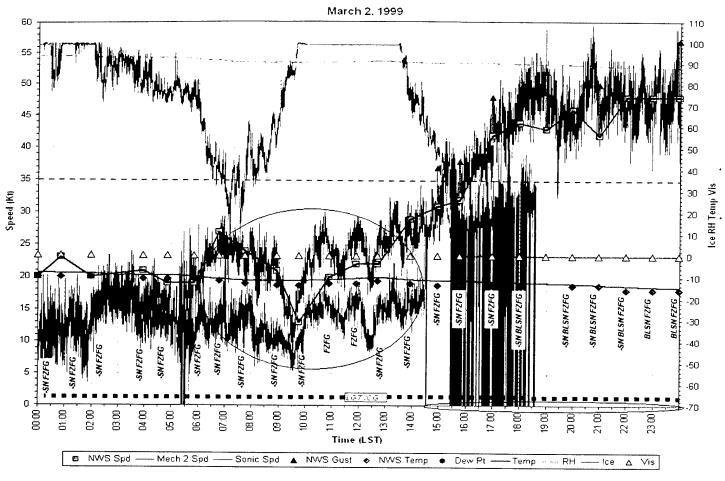
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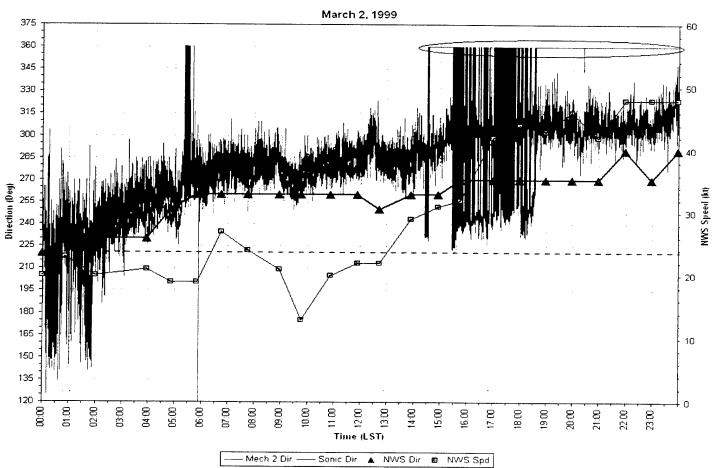




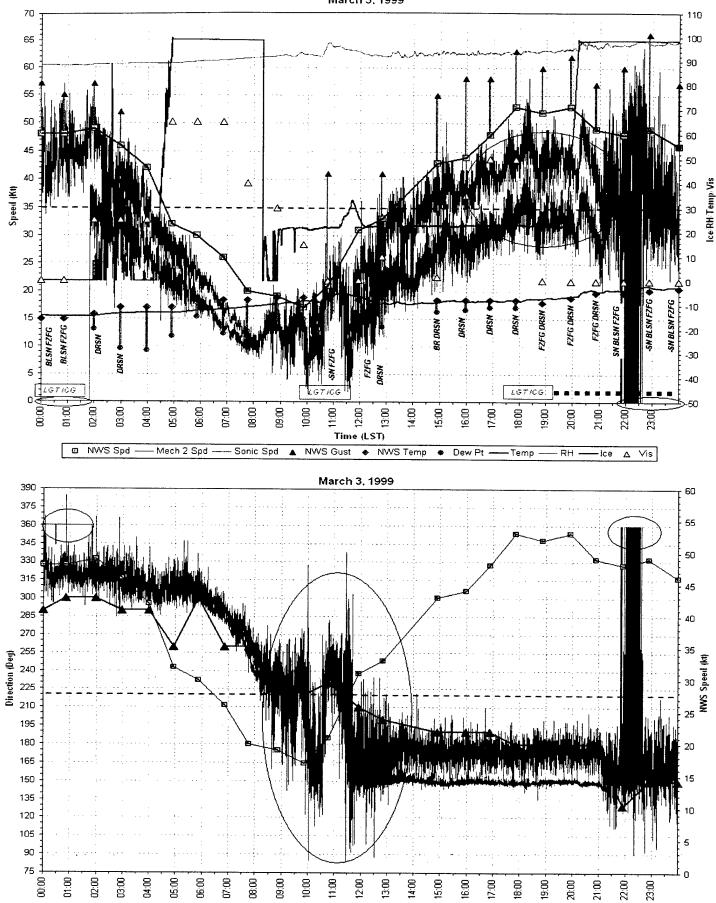












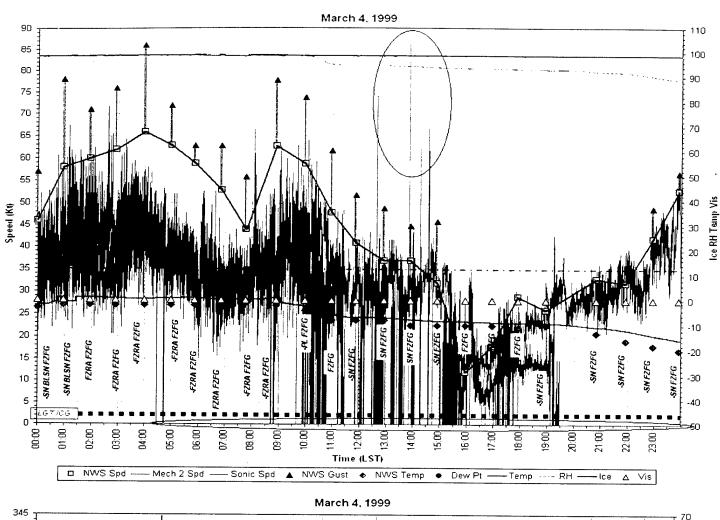
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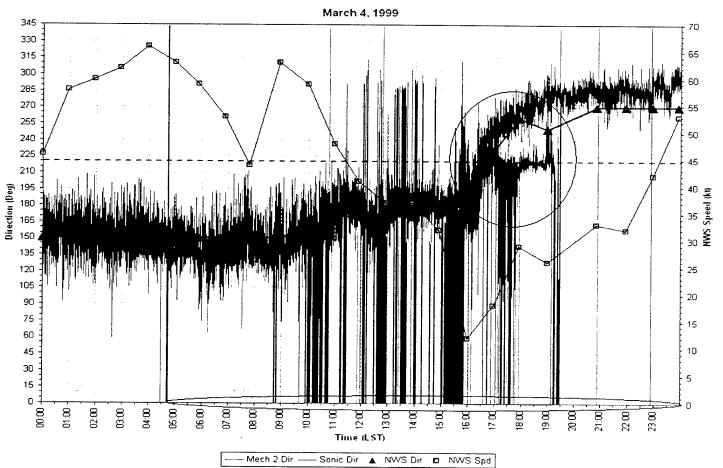
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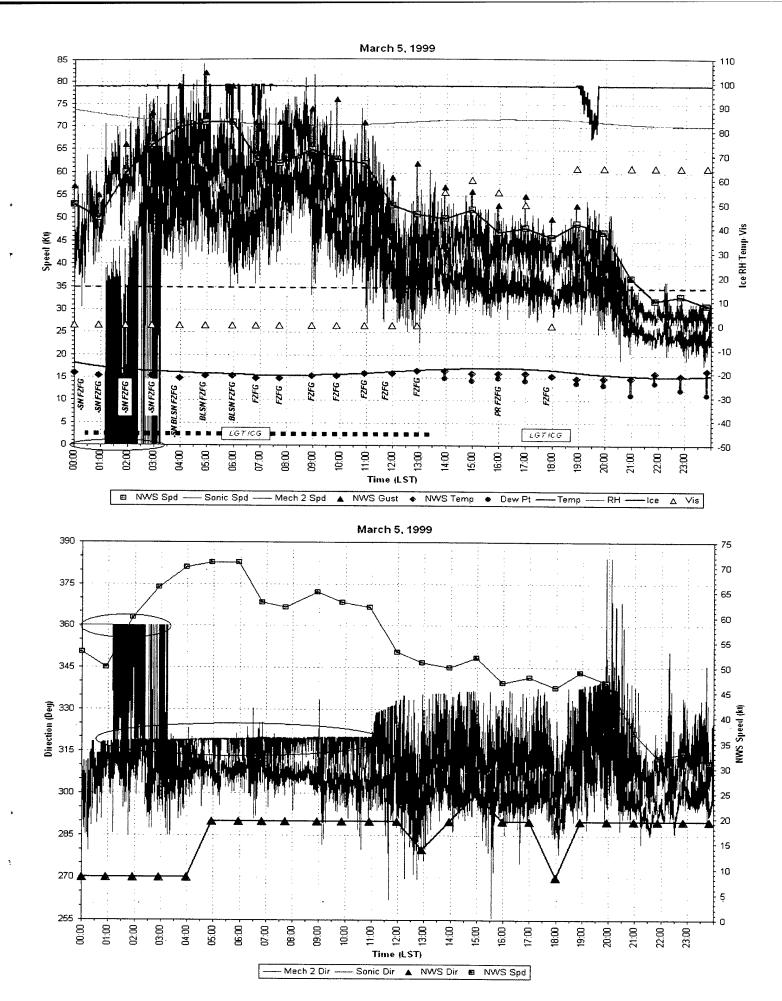
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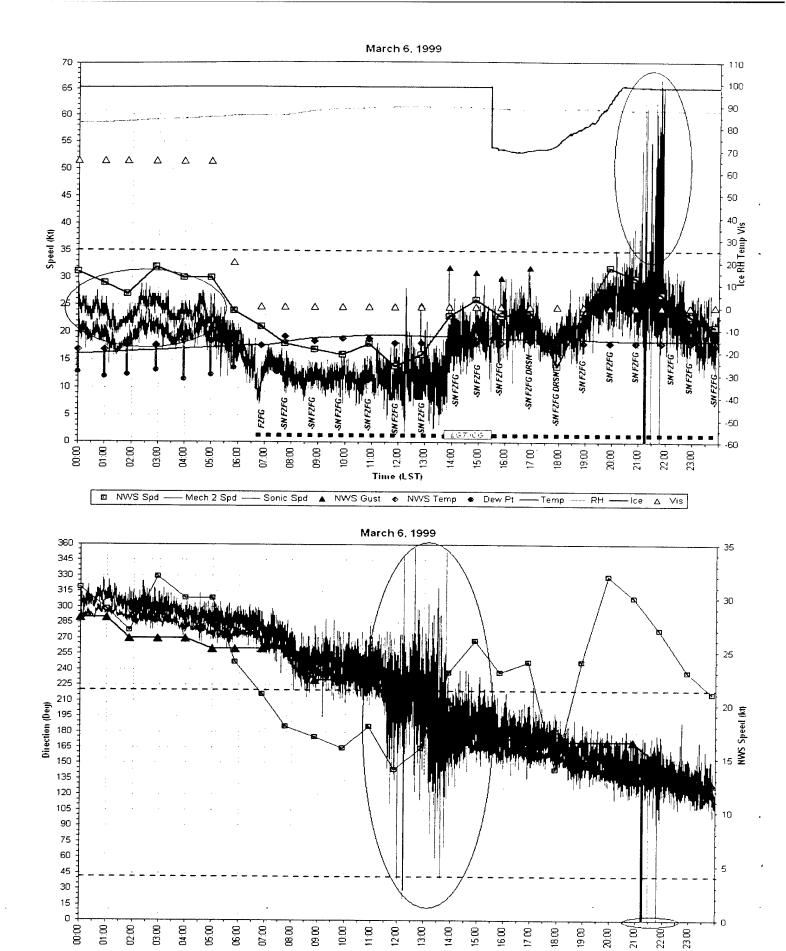
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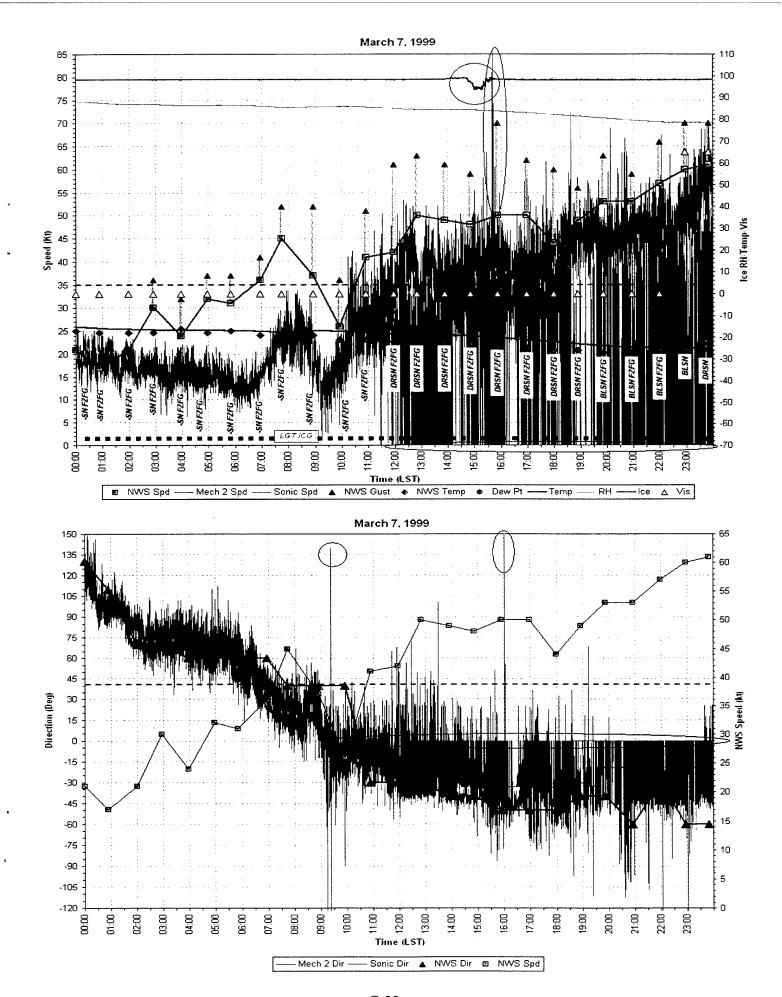


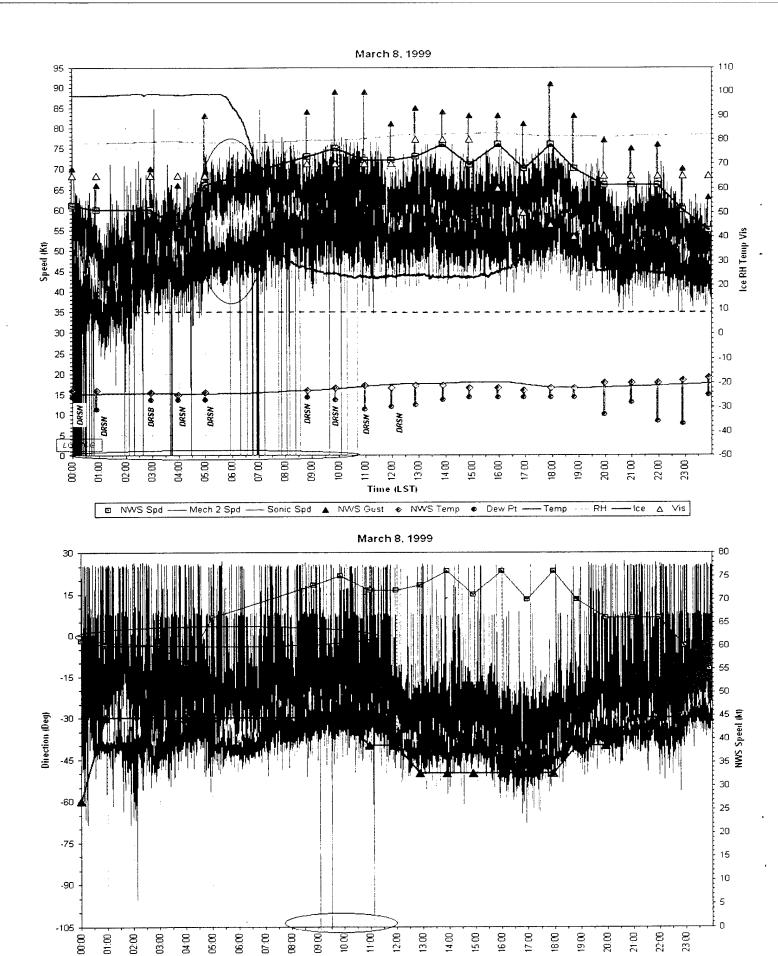


Mech 2 Dir ----

Time (LST)

– Sonic Dir ▲ NWS Dir 🛛 NWS Spd





Time (LST)

- Mech 2 Dir ---- Sonic Dir A NWS Dir D NWS Spd



